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# Low-, Wide- Voltage Battery Front-End DC/DC Converter Single-Cell Li-lon, Ni-Rich, Si-Anode Applications

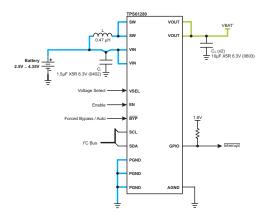
Check for Samples: TPS61280, TPS61281, TPS61282

#### **FEATURES**

- 95% Efficiency at 2.3MHz Operation
- 2µA Quiescent Current in Low Io Pass-Through Mode
- Wide V<sub>IN</sub> Range From 2.3V to 4.8V
- $I_{OUT} \ge 4A$  (Peak) at  $V_{OUT} = 3.35V$ ,  $V_{IN} \ge 2.65V$
- Integrated Pass-Through Mode (35mΩ)
- **Programmable Valley Inductor Current Limit** and Output Voltage
- **True Pass-Through Mode During Shutdown**
- Best-in-Class Line and Load Transient
- Low-Ripple Light-Load PFM Mode
- In-Situ Customization with On-Chip E<sup>2</sup>PROM (Write Protect)
- **Two Interface Options:** 
  - I<sup>2</sup>C Compatible I/F up to 3.4Mbps (TPS61280)
  - Simple I/O Logic Control Interface (TPS6128x)
- Thermal Shutdown and Overload Protection
- Total Solution Size <20mm<sup>2</sup>, Sub 1-mm Profile

#### **APPLICATIONS**

- Single-Cell Ni-Rich, Si-Anode, Li-Ion, LiFePO4 **Smart-Phones or Tablet PCs**
- 2.5G/3G/4G Mini-Module Data Cards
- **Current Limited Applications Featuring High Peak Power Loads**



#### DESCRIPTION

The TPS6128x device provides a power supply solution for products powered by either by a Li-lon, Nickel-Rich, Silicon Anode, Li-Ion or LiFePO4 battery. The voltage range is optimized for single-cell portable applications like in smart-phones or tablet PCs.

Used as a high-power pre-regulator, the TPS6128x extends the battery run-time and overcomes input current- and voltage limitations of the powered system.

While in shutdown, the TPS6128x operates in a true pass-through mode with only 2µA quiescent consumption for longest battery shelf life.

During operation, when the battery is at a good stateof-charge, a low-ohmic, high-efficient integrated passthrough path connects the battery to the powered system.

If the battery gets to a lower state of charge and its voltage becomes lower than the desired minimum system voltage, the device seamlessly transits into boost mode to utilize the full battery capacity. TPS6128x device supports more than 4A pulsed load current even from a deeply discharged battery. In this mode of operation, the TPS6128x enables the utilization of the full battery capacity: A high batterycut-off voltage originated by powered components with a high minimum input voltage is overcome; new battery chemistries can be fully discharged; high current pulses forcing the system into shutdown are buffered by the device seamlessly transitioning between boost and by-pass mode back and forth.

This has significant impact on the battery on-time and translates into either a longer use-time and better user-experience at an equal battery capacity or into reduced battery costs at similar use-times.

The TPS6128x operates in synchronous, 2.3MHz boost mode and enters power-save mode operation (PFM) at light load currents to maintain high efficiency over the entire load current range.

The TPS6128x offers a very small solution size (<20mm<sup>2</sup>) due to minimum amount of external components, enabling the use of small inductors and input capacitors, available as a 16-pin chip-scale package (CSP).

Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet. I<sup>2</sup>C is a trademark of NXP Semiconductors.

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These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

#### **AVAILABLE DEVICE OPTIONS**

PART NUMBER <sup>(1)</sup>	S	ORDERING <sup>(2)</sup>	PACKAGE MARKING CHIP CODE	
	.2	DC/DC boost / bypass threshold = 3.15V (Vsel = L)		
TPS61280	I <sup>2</sup> C Control Interface User Prog. E <sup>2</sup> PROM Settings	DC/DC boost / bypass threshold = 3.35V (Vsel = H)	TPS61280YFF	TPS61280
	Cool 1 log. E 1 from Counigo	Valley inductor current limit = 3A		
	Simple Logic Control Interface	DC/DC boost / bypass threshold = 3.15V (Vsel = L)	TPS61281YFF	
TPS61281		DC/DC boost / bypass threshold = 3.35V (Vsel = H)		TPS61281
		Valley inductor current limit = 3A		
		DC/DC boost / bypass threshold = 3.3V (Vsel = L)		
TPS61282	Simple Logic Control Interface	DC/DC boost / bypass threshold = 3.5V (Vsel = H)	TPS61282YFF	TPS61282
		Valley inductor current limit = 4A		

<sup>(1)</sup> For the most current package and ordering information, see the Package Option Addendum at the end of this document, or see the TI website at www.ti.com.

#### **ABSOLUTE MAXIMUM RATINGS**

over operating free-air temperature range (unless otherwise noted)(1)

				UNIT
	Voltage at VOUT <sup>(2)</sup>	DC	-0.3 to 4.7	V
	Voltage at VIN <sup>(2)</sup> , EN <sup>(2)</sup> , VSEL <sup>(2)</sup> , nBYP <sup>(2)</sup> , PG <sup>(2)</sup> , GPIO <sup>(2)</sup>	DC	-0.3 to 5.2	V
Input voltage	Voltage at SCL <sup>(2)</sup> , SDA <sup>(2)</sup> MODE <sup>(2)</sup>	DC	-0.3 to 3.6	V
	Voltage at SW <sup>(2)</sup>	DC	-0.3 to 4.7	V
	Vollage at SWV	Transient: 2 ns, 2.3 MHz	-0.3 to 5.5	V
	Differential voltage between VIN and VOUT	-0.3 to 4	V	
Innut aurrant	Continuous average current into SW (3)	1.8	Α	
Input current	Peak current into SW (4)	5.5	Α	
Power dissipation			Internally li	mited
	Operating temperature range, T <sub>A</sub> <sup>(5)</sup>		-40 to 85	°C
Temperature range	Operating virtual junction, T <sub>J</sub>	-40 to 150	°C	
	Storage temperature range, T <sub>stg</sub>	-65 to 150	°C	
	Human Body Model - (HBM)	2000	V	
ESD rating	Charge Device Model - (CDM)	1000	V	
	Machine Model - (MM)	100	V	

<sup>(1)</sup> Stresses beyond those listed under *absolute maximum ratings* may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under *recommended operating conditions* is not implied. Exposure to absolute-maximum-rated conditions for extended periods my affect device reliability.

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<sup>(2)</sup> The YFF package is available in tape and reel. Add a R suffix (e.g. TPS61280YFFR) to order quantities of 3000 parts. Add a T suffix (e.g. TPS61280YFFT) to order quantities of 250 parts.

<sup>(2)</sup> All voltages are with respect to network ground terminal.

<sup>(3)</sup> Limit the junction temperature to 105°C for continuous operation at maximum output power.

<sup>(4)</sup> Limit the junction temperature to 105°C for 15% duty cycle operation.

<sup>(5)</sup> In applications where high power dissipation and/or poor package thermal resistance is present, the maximum ambient temperature may have to be derated. Maximum ambient temperature (T<sub>A(max)</sub>) is dependent on the maximum operating junction temperature (T<sub>J(max)</sub>), the maximum power dissipation of the device in the application (P<sub>D(max)</sub>), and the junction-to-ambient thermal resistance of the part/package in the application (θ<sub>JA</sub>), as given by the following equation: T<sub>A(max)</sub> = T<sub>J(max)</sub> – (θ<sub>JA</sub> X P<sub>D(max)</sub>). To achieve optimum performance, it is recommended to operate the device with a maximum junction temperature of 105°C.

#### THERMAL INFORMATION

		TPS6128x	
	THERMAL METRIC <sup>(1)</sup>	YFF	UNIT
		16 PINS	
$\theta_{JA}$	Junction-to-ambient thermal resistance	78	
$\theta_{JCtop}$	Junction-to-case (top) thermal resistance	0.6	
$\theta_{JB}$	Junction-to-board thermal resistance	13	°C/W
ΨЈТ	Junction-to-top characterization parameter	2.4	C/VV
ΨЈВ	Junction-to-board characterization parameter	13	
$\theta_{JCbot}$	Junction-to-case (bottom) thermal resistance	n/a	

<sup>(1)</sup> For more information about traditional and new thermal metrics, see the IC Package Thermal Metrics application report, SPRA953.

#### RECOMMENDED OPERATING CONDITIONS

		MIN	NOM	MAX	UNIT
	Input voltage range	2.30		4.85	V
VI	Input voltage range for in-situ customization by E <sup>2</sup> PROM write operation	3.4	3.5	3.6	V
L	Inductance	200	470	800	nΗ
Co	Output capacitance	9	13	100	μF
IL_Start_ Max	Maximum load current during start-up	250			mA
T <sub>A</sub>	Ambient temperature	-40		85	°C
T <sub>J</sub>	Operating junction temperature	-40		125	°C

#### **ELECTRICAL CHARACTERISTICS**

Minimum and maximum values are at  $V_{IN} = 2.3V$  to 4.85V,  $V_{OUT} = 3.4V$  (or  $V_{IN}$ , whichever is higher), EN = 1.8V, VSEL = 1.8V, nBYP = 1.8V,  $-40^{\circ}C \le T_{J} \le 125^{\circ}C$ ; Circuit of Parameter Measurement Information section (unless otherwise noted). Typical values are at  $V_{IN} = 3.2V$ ,  $V_{OUT} = 3.4V$ , EN = 1.8V,  $T_{J} = 25^{\circ}C$  (unless otherwise noted).

PARAMETER			TEST CONDITIONS		MIN	TYP	MAX	UNIT	
SUPPL	Y CURRENT								
lα		switching	$I_{OUT} = 0$ mA, $V_{IN} = 3.2$ V, $V_{OUT} =$			47	65	μΑ	
	Operating quiescent current into V <sub>IN</sub>	TPS6128x	Pass-through mode (auto) EN = 1.8V, nBYP = 1.8V, V <sub>IN</sub> = 3.6V			27	42	μΑ	
		TP56128X	Pass-through mode (forced) EN = 1.8V, nBYP = AGND, V <sub>OUT</sub> = 3.6V	-40°C ≤ T <sub>J</sub> ≤ 85°C		15	25	μΑ	
	Operating quiescent current into V <sub>OUT</sub>			DC/DC boost mode. Device not switching $I_{OUT} = 0$ mA, $V_{IN} = 3.2$ V, $V_{OUT} = 3.4$ V			8.5	19	μΑ
	Chutdown ourrent	TDC6420v	$EN = 0V, nBYP = 0V, V_{IN} = 3.6V$			2.6	6.0	μΑ	
I <sub>SD</sub>	Shutdown current	TPS6128x	$EN = 0V$ , $nBYP = 1.8V$ , $V_{IN} = 3.6V$			8.5	20	μΑ	
V	Llader veltege leekeut threehold	TPS6128x	Falling			2.0	2.1	V	
$V_{UVLO}$	Under-voltage lockout threshold	1P30120X	Hysteresis			0.1		V	
EN, VS	EL, nBYP, MODE, SDA, SCL, GI	PIO, PG		<u> </u>					
V <sub>IL</sub>	Low-level input voltage	TDCC400					0.4	V	
V <sub>IH</sub>	High-level input voltage	TPS6128x			1.2			V	

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#### **ELECTRICAL CHARACTERISTICS (continued)**

Minimum and maximum values are at  $V_{IN}=2.3V$  to 4.85V,  $V_{OUT}=3.4V$  (or  $V_{IN}$ , whichever is higher), EN = 1.8V, VSEL = 1.8V, nBYP = 1.8V,  $-40^{\circ}$ C  $\leq T_{J} \leq 125^{\circ}$ C; Circuit of Parameter Measurement Information section (unless otherwise noted). Typical values are at  $V_{IN}=3.2V$ ,  $V_{OUT}=3.4V$ , EN = 1.8V,  $T_{J}=25^{\circ}$ C (unless otherwise noted).

PARAMETER			TEST CONDITIONS		MIN	TYP	MAX	UNIT
	Low-level output voltage (SDA)		I <sub>OL</sub> = 8mA				0.3	V
$V_{OL}$	Low-level output voltage (GPIO)	TPS61280	I <sub>OL</sub> = 8mA, GPIOCFG = 0				0.3	V
	Low-level output voltage (PG)	TPS6128x	I <sub>OL</sub> = 8mA				0.3	V
$R_{PD}$	EN, VSEL, nBYP, pull-down resistance	TPS6128x	Input ≤ 0.4 V			300		kΩ
0	EN, VSEL, nBYP, MODE, PG input capacitance	TPS6128x	land to accompate the ACND on V			9		pF
C <sub>IN</sub>	SDA, SCL, GPIO input capacitance	TPS61280	Input connected to AGND or V <sub>IN</sub>			9		pF
V	Dower good throubold	TDC6400v	Rising V <sub>OUT</sub>			0.95 x V <sub>OUT</sub>		
V <sub>THPG</sub>	Power good threshold	TPS6128x	Falling V <sub>OUT</sub>			0.9 x V <sub>OUT</sub>		
I <sub>lkg</sub>	Innut lookogo ourront	TDC6420v	Input connected to AGND	–40°C ≤ T <sub>J</sub>		0		μΑ
	Input leakage current	TPS6128x	Input connected V <sub>IN</sub>	≤ 85°C			0.5	μΑ
OUTPL	JT							
V <sub>OUT_</sub>	Threshold DC voltage accuracy	TPS6128x	No load. Open loop		-1.5		+1.5	%
	Pagulated DC valtage accuracy	TDC6420v	$2.65\text{V} \le \text{V}_{\text{IN}} \le \text{V}_{\text{OUT\_TH}} - 150\text{mV}$ $\text{I}_{\text{OUT}} = 0\text{mA}$ PWM operation.		-2.0		+2.0	%
V <sub>OUT</sub>	Regulated DC voltage accuracy TPS61	TPS6128x	$2.65V \le V_{IN} \le V_{OUT\_TH} - 150mV$ $I_{OUT} = 0mA$ PFM/PWM operation		-2.0		+4.0	%
۸۱/	Power-save mode output ripple voltage	TPS6128x	PFM operation, I <sub>OUT</sub> = 1mA			30		mVpk
$\Delta V_{OUT}$	PWM mode output ripple voltage	1P30120X	PWM operation, I <sub>OUT</sub> = 500mA			15		mVpk
POWE	R SWITCH			•			•	
	Low-side switch MOSFET on resistance		V <sub>IN</sub> = 3.2, V <sub>OUT</sub> = 3.5V			45	80	mΩ
r <sub>DS(on)</sub>	High-side rectifier MOSFET on resistance	TPS6128x	V <sub>IN</sub> = 3.2V, V <sub>OUT</sub> = 3.5V			40	70	mΩ
·D3(0II)	High-side pass-through MOSFET on resistance		V <sub>IN</sub> = 3.2V, V <sub>OUT</sub> = 3.5V			35	60	mΩ
	Reverse leakage current into SW		EN = AGND, $V_{IN} = V_{OUT} = SW = 3.5$ -40°C $\leq T_J \leq 85$ °C	5V		0.1	2	μΑ
I <sub>lkg</sub> Reverse leakage current into VOUT		TPS6128x	$\begin{split} &EN = nBYP = VIN, \ V_{IN} = 2.9V, \ V_{OUT} \\ &= 0V \\ &device \ not \ switching \\ &-40^{\circ}C \le T_{J} \le 85^{\circ}C \end{split}$	= 4.4V, V <sub>SW</sub>		0.1 1	2	μΑ
I <sub>SINK</sub>	VOUT sink capability	TPS6128x	$EN = AGND$ , $V_{OUT} \le 3.6V$ , $I_{OUT} = -10$	)mA			0.3	V



#### **ELECTRICAL CHARACTERISTICS (continued)**

Minimum and maximum values are at  $V_{IN}=2.3V$  to 4.85V,  $V_{OUT}=3.4V$  (or  $V_{IN}$ , whichever is higher), EN = 1.8V, VSEL = 1.8V, nBYP = 1.8V,  $-40^{\circ}$ C  $\leq T_{J} \leq 125^{\circ}$ C; Circuit of Parameter Measurement Information section (unless otherwise noted). Typical values are at  $V_{IN}=3.2V$ ,  $V_{OUT}=3.4V$ , EN = 1.8V,  $T_{J}=25^{\circ}$ C (unless otherwise noted).

	PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
	Valley inductor current limit	TPS61280 TPS61281	$V_{\rm IN}$ = 2.9V, $V_{\rm OUT}$ = 3.5V, $-40^{\circ}{\rm C} \le {\rm T_J} \le 125^{\circ}{\rm C}$ , auto PFM/PWM	2475	3000	3525	mA
	Valley inductor current limit	TPS61282	$V_{\text{IN}}$ = 2.9V, $V_{\text{OUT}}$ = 3.5V, -40°C $\leq$ T <sub>J</sub> $\leq$ 125°C, auto PFM/PWM	3300	4000	4700	mA
	B	$EN = nBYP = GND, V_{IN} = 3.2V$		5000		mA	
	Pass through mode current limit	TPS6128x	EN = VIN, nBYP = don't care , V <sub>IN</sub> = 3.2V	5600	7400	9100	mA
	Pre-charge mode current limit (linear mode, phase 1)	TDC6420v	V V 200mV	500	650		mA
	Pre-charge mode current limit (linear mode, phase 2)	TPS6128x	$V_{IN} - V_{OUT} >= 300 \text{mV}$		2000		mA
OSCIL	LATOR	•					
fosc	Oscillator frequency	TPS6128x	$V_{IN} = 2.7V, V_{OUT} = 3.5$		2.3		MHz
THERM	THERMAL SHUTDOWN, HOT DIE DETECTOR						
	Thermal shutdown <sup>(1)</sup>	TPS6128x		140	160		°C
	Hot die detector accuracy <sup>(1)</sup>	TPS61280		-10	105	+10	°C

<sup>(1)</sup> Verified by characterization. Not tested in production.

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## **ELECTRICAL CHARACTERISTICS (continued)**

Minimum and maximum values are at  $V_{IN}=2.3V$  to 4.85V,  $V_{OUT}=3.4V$  (or  $V_{IN}$ , whichever is higher), EN = 1.8V, VSEL = 1.8V, nBYP = 1.8V,  $-40^{\circ}C \le T_{J} \le 125^{\circ}C$ ; Circuit of Parameter Measurement Information section (unless otherwise noted). Typical values are at  $V_{IN}=3.2V$ ,  $V_{OUT}=3.4V$ , EN = 1.8V,  $T_{J}=25^{\circ}C$  (unless otherwise noted).

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
TIMING						
Start-up time	TPS6128x	$\begin{aligned} &V_{\text{IN}} = 3.2\text{V}, \ \text{VOUT\_TH} = 01011 \ (3.4\text{V}), \ \text{R}_{\text{LOAD}} = \\ &50\Omega \end{aligned}$ Time from active $V_{\text{IN}}$ to $V_{\text{OUT}}$ settled		500		μs
GPIO rise time <sup>(2)</sup>	TPS61280				200	ns

<sup>(2)</sup> Verified by characterization. Not tested in production.

## I<sup>2</sup>C INTERFACE TIMING CHARACTERISTICS<sup>(1)</sup>

	PARAMETER	TEST CONDITIONS	MIN	MAX	UNIT
		Standard mode		100	kHz
		Fast mode		400	kHz
		Fast mode plus		1	MHz
f <sub>(SCL)</sub>	SCL Clock Frequency	High-speed mode (write operation), C <sub>B</sub> – 100 pF max		3.4	MHz
		High-speed mode (read operation), C <sub>B</sub> – 100 pF max		3.4	MHz
		High-speed mode (write operation), C <sub>B</sub> – 400 pF max		1.7	MHz
		High-speed mode (read operation), C <sub>B</sub> – 400 pF max		1.7	MHz
		Standard mode	4.7		μs
t <sub>BUF</sub>	Bus Free Time Between a STOP and START Condition	Fast mode	1.3		μs
	CITACT CONGINOT	Fast mode plus	0.5		μs
		Standard mode	4		μs
	Hold Time (Repeated) START	Fast mode	600		ns
t <sub>HD</sub> , t <sub>STA</sub>	Condition	Fast mode plus	260		ns
		High-speed mode	160		ns
	LOW Period of the SCL Clock	Standard mode	4.7		μs
		Fast mode	1.3		μs
$t_{LOW}$		Fast mode plus	0.5		μs
		High-speed mode, C <sub>B</sub> – 100 pF max	160		ns
		High-speed mode, C <sub>B</sub> – 400 pF max	320		ns
		Standard mode	4		μs
		Fast mode	600		ns
t <sub>HIGH</sub>	HIGH Period of the SCL Clock	Fast mode plus	260		ns
		High-speed mode, C <sub>B</sub> – 100 pF max	60		ns
		High-speed mode, C <sub>B</sub> – 400 pF max	120		ns
		Standard mode	4.7		μs
	Setup Time for a Repeated START	Fast mode	600		ns
t <sub>SU</sub> , t <sub>STA</sub>	Condition	Fast mode plus	260		ns
		High-speed mode	160		ns
		Standard mode	250		ns
	Data Satura Tima	Fast mode	100		ns
<sup>t</sup> SU <sup>, t</sup> DAT	Data Setup Time	Fast mode plus	50		ns
		High-speed mode	10		ns

# I<sup>2</sup>C INTERFACE TIMING CHARACTERISTICS<sup>(1)</sup> (continued)

	PARAMETER	TEST CONDITIONS	MIN	MAX	UNIT
		Standard mode	0	3.45	μs
		Fast mode	0	0.9	μs
HD, t <sub>DAT</sub>	Data Hold Time	Fast mode plus	0		μs
		High-speed mode, C <sub>B</sub> – 100 pF max	0	70	ns
		High-speed mode, C <sub>B</sub> – 400 pF max	0	150	ns
		Standard mode		1000	ns
		Fast mode	20 + 0.1 C <sub>B</sub>	300	ns
RCL	Rise Time of SCL Signal	Fast mode plus		120	ns
		High-speed mode, C <sub>B</sub> – 100 pF max	10	40	ns
		High-speed mode, C <sub>B</sub> – 400 pF max	20	80	ns
		Standard mode	20 + 0.1 C <sub>B</sub>	1000	ns
	Rise Time of SCL Signal After a	Fast mode	20 + 0.1 C <sub>B</sub>	300	ns
RCL1	Repeated START Condition and After	Fast mode plus		120	ns
	an Acknowledge BIT	High-speed mode, C <sub>B</sub> – 100 pF max	10	80	ns
		High-speed mode, C <sub>B</sub> – 400 pF max	20	160	ns
		Standard mode	20 + 0.1 C <sub>B</sub>	300	ns
		Fast mode		300	ns
FCL	Fall Time of SCL Signal	Fast mode plus		120	ns
. 02		High-speed mode, C <sub>B</sub> – 100 pF max	10	40	ns
		High-speed mode, C <sub>B</sub> – 400 pF max	20	80	ns
		Standard mode		1000	ns
		Fast mode	20 + 0.1 C <sub>B</sub>	300	ns
RDA	Rise Time of SDA Signal	Fast mode plus		120	ns
		High-speed mode, C <sub>B</sub> – 100 pF max	10	80	ns
		High-speed mode, C <sub>B</sub> – 400 pF max	20	160	ns
		Standard mode		300	ns
		Fast mode	20 + 0.1 C <sub>B</sub>	300	ns
FDA	Fall Time of SDA Signal	Fast mode plus		120	ns
		High-speed mode, C <sub>B</sub> – 100 pF max	10	80	ns
		High-speed mode, C <sub>B</sub> – 400 pF max	20	160	ns
		Standard mode	4		μs
	0 / 7 / 0700 0 ///	Fast mode	600		ns
SU, <sup>t</sup> STO	Setup Time of STOP Condition	Fast mode plus	260		ns
		High-Speed mode	160		ns
		Standard mode		400	pF
	0 " 1 1/ 05 1 100	Fast mode		400	pF
$C_{B}$	Capacitive Load for SDA and SCL	Fast mode plus		550	pF
		High-Speed mode		400	pF

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# TEXAS INSTRUMENTS

#### I<sup>2</sup>C TIMING DIAGRAMS

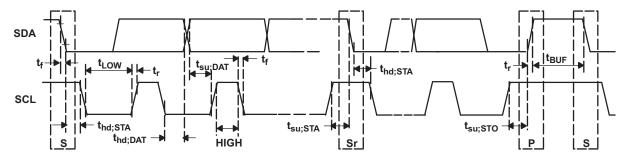
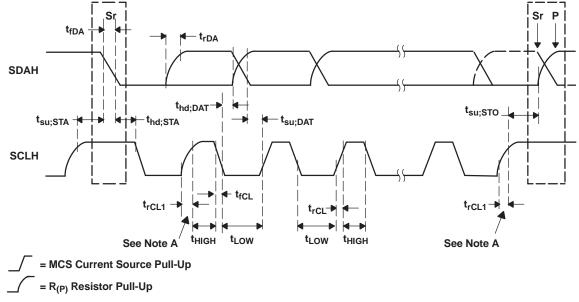


Figure 1. Serial Interface Timing Diagram for Standard-, Fast-, Fast-Mode Plus



Note A: First rising edge of the SCLH signal after Sr and after each acknowledge bit.

Figure 2. Serial Interface Timing Diagram for H/S-Mode

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#### **DEVICE INFORMATION**

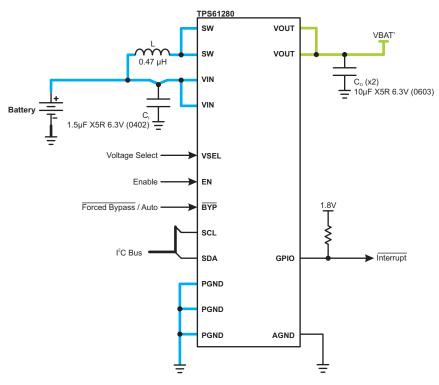


Figure 3. TPS61280, Device Overview

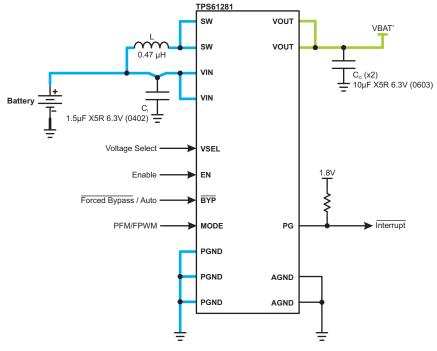
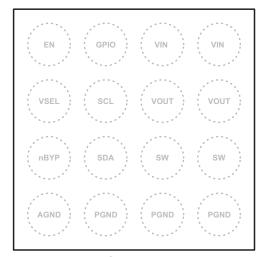


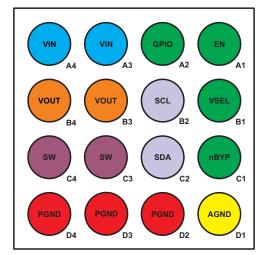
Figure 4. TPS6128x, Device Overview

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# **PIN ASSIGNMENTS (TPS61280)**





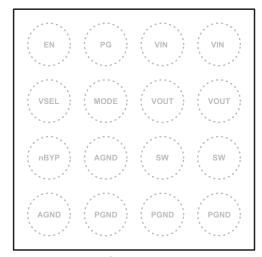
**TOP VIEW** 

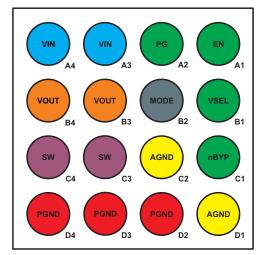
**BOTTOM VIEW** 

Table 1. PIN FUNCTIONS (TPS61280)

PIN		1/0	DECORIDATION
NAME	NO.	I/O	DESCRIPTION
VIN	A3, A4	I	Power supply input.
VOUT	B3, B4	0	Boost converter output.
			This is the enable pin of the device. On the rising edge of the enable pin, all the registers are reset with their default values. This input must not be left floating and must be terminated.
EN	A1	I	EN = Low: The device is forced into shutdown mode and the I2C control interface is disabled. Depending on the logic level applied to the nBYP input, the converter can either be forced in pass-through mode or it's output can be regulated to a minimum level so as to limit the input-to-output voltage difference to less than 3.6V (typ). The current consumption is reduced to a few $\mu$ A. For more details, refer to Table 5.
			EN = High: The device is operating normally featuring automatic dc/dc boost, pass-through mode transition. For more details, refer to Table 5.
			This pin can either be configured as a input (mode selection) or as dual role input/open-drain output (nRST/nFAULT) pin. Per default, the pin is configured as nRST/nFAULT input/output. The input must not be left floating and must be terminated.
			Manual Reset Input: Drive nRST/nFAULT low to initiate a reset of the converter's output. nRST/nFAULT controls a falling edge-triggered sequence consisting of a discharge phase of the capacitance located at the converter's output followed by a start-up phase.
GPIO	A2	I/O	Fault Output (open-drain interrupt signal to host): Indicates that a fault has occurred (e.g. thermal shutdown, output voltage out of limits, current limit triggered etc). To signal such an event, the device generates a falling edge-triggered interrupt by driving a negative pulse onto the GPIO line and then releases the line to its inactive state.
			Mode selection input = Low: The device is operating in regulated frequency pulse width modulation mode (PWM) at high-load currents and in pulse frequency modulation mode (PFM) at light load currents.
			Mode selection input = High: Low-noise mode enabled, regulated frequency PWM operation forced.
VSEL	B1	I	VSEL signal is primarily used to set the output voltage dc/dc boost, pass-through threshold. This pin must not be left floating and must be terminated.
nBYP	C1	I	A logic low level on the nBYP input forces the device in pass-through mode. For more details, refer to . This pin must not be left floating and must be terminated.
SCL	B2	I	Serial interface clock line. This pin must not be left floating and must be terminated.
SDA	C2	I/O	Serial interface address/data line. This pin must not be left floating and must be terminated.
SW	C3, C4	I/O	Inductor connection. Drain of the internal power MOSFET. Connect to the switched side of the inductor.
PGND	D2, D3, D4		Power ground pin.
AGND	D1		Analog ground pin. This is the signal ground reference for the IC.

# PIN ASSIGNMENTS (TPS6128x)





**TOP VIEW** 

**BOTTOM VIEW** 

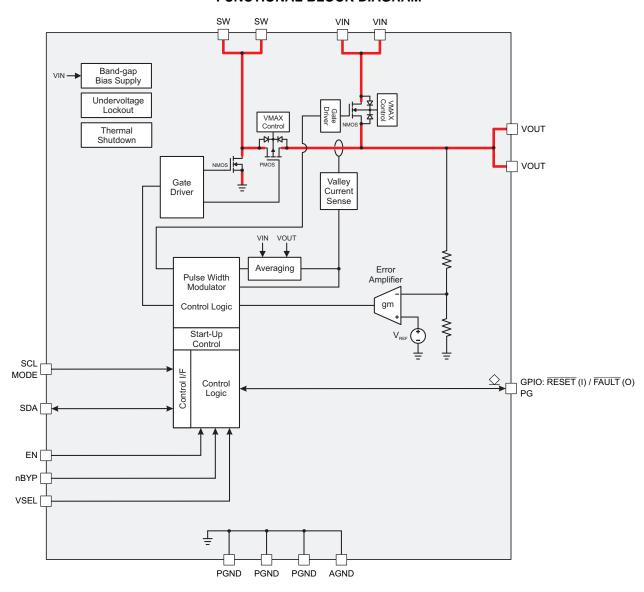
Table 2. PIN FUNCTIONS (TPS6128x)

PIN		1/0	DESCRIPTION
NAME	NO.	1/0	DESCRIPTION
VIN	A3, A4	I	Power supply input.
VOUT	B3, B4	0	Boost converter output.
			This is the enable pin of the device. On the rising edge of the enable pin, all the registers are reset with their default values. This input must not be left floating and must be terminated.
EN	A1	I	EN = Low: The device is forced into shutdown mode. Depending on the logic level applied to the nBYP input, the converter can either be forced in pass-through mode or it's output can be regulated to a minimum level so as to limit the input-to-output voltage difference to less than 3.6V (typ). The current consumption is reduced to a few $\mu$ A. For more details, refer to .
			EN = High: The device is operating normally featuring automatic dc/dc boost, pass-through mode transition. For more details, refer to .
PG	A2	0	Power-Good Output (open-drain output to host): A logic high on the PG output indicates that the converter's output voltage is within its regulation limits. A logic low indicates a fault has occurred (e.g. thermal shutdown, output voltage out of limits, current limit triggered etc). The PG signal is deasserted automatically once the IC resumes proper operation.
VSEL	B1	I	VSEL signal is primarily used to set the output voltage dc/dc boost, pass-through threshold. This pin must not be left floating and must be terminated.
nBYP	C1	ı	A logic low level on the nBYP input forces the device in pass-through mode. For more details, refer to . This pin must not be left floating and must be terminated.
			This is the mode selection pin of the device. This pin must not be left floating, must be terminated and can be connected to AGND. During start-up this pin must be held low. Once the output voltage settled and PG pin indicates that the converter's output voltage is within its regulation limits the device can be forced in PWM mode operation by applying a high level on this pin.
MODE	B2	I	MODE = Low: The device is operating in regulated frequency pulse width modulation mode (PWM) at high-load currents and in pulse frequency modulation mode (PFM) at light load currents. This pin must be held low during device start-up.
			MODE = High: Low-noise mode enabled, regulated frequency PWM operation forced.
sw	C3, C4	I/O	Inductor connection. Drain of the internal power MOSFET. Connect to the switched side of the inductor.
PGND	D2, D3, D4		Power ground pin.
AGND	C2, D1		Analog ground pin. This is the signal ground reference for the IC.

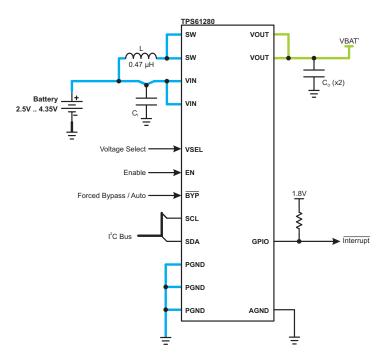
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# Instruments

#### **FUNCTIONAL BLOCK DIAGRAM**



# PARAMETER MEASUREMENT INFORMATION



**Table 3. List of Components** 

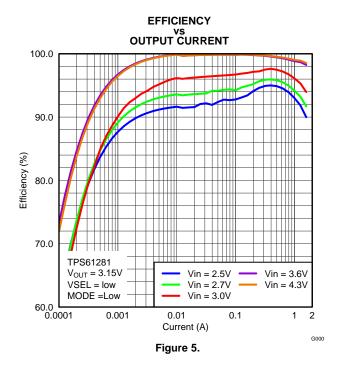
REFERENCE	DESCRIPTION	PART NUMBER, MANUFACTURER
Cı	1.5µF, 6.3V, 0402, X5R ceramic	GRM155R60J155ME80D, muRata
Co	10μF, 6.3V, 0603, X5R ceramic	GRM188R60J106ME84, muRata
L	470nH, 47mOhm, 2.5mm x 2.0mm x 1.2mm	DFE252012CR470 , TOKO

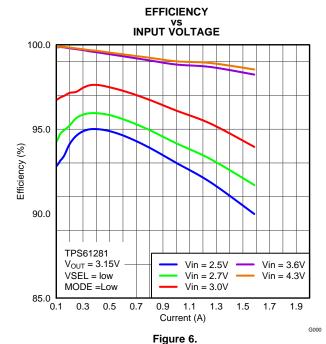
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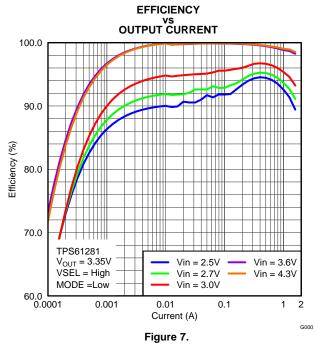
# TYPICAL CHARACTERISTICS TABLE OF GRAPHS

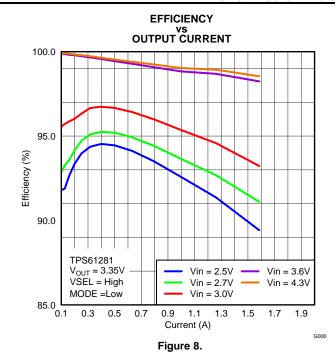
			FIGURE
η	Efficiency	vs Output current	7, 8, 9, 10, 11, 12
Vo	DC output voltage	vs Output current	13, 14, 15, 16, 17, 18, 19, 20
· ·	, ,	vs Input voltage	21, 22, 23, 24
lo	Maximum output current	vs Input voltage	25
	Boost to Pass-Through Mode Exit / Entry	vs Output current	26
	Dynamic Voltage Management (VSEL)	vs Input voltage	27, 28, 29, 30
I <sub>LIM</sub>	Line TransientResponse		31, 32
	Load Transient Response		33, 34, 35, 36, 37
	Start-up		38, 39

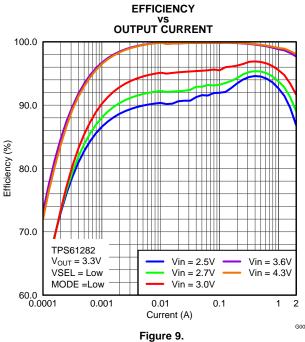




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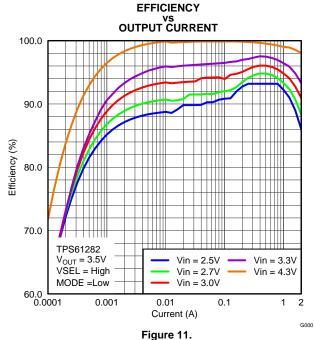


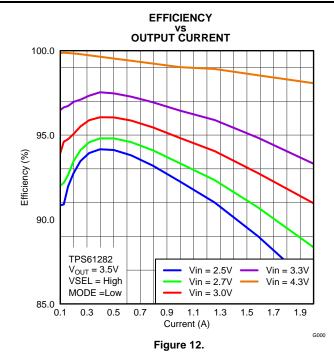
**EFFICIENCY** vs OUTPUT CURRENT 100.0 95.0 Efficiency (%) 90.0 TPS61282 V<sub>OUT</sub> = 3.3V VSEL = Low Vin = 2.5V Vin = 3.3V Vin = 2.7VMODE =Low Vin = 3.0V85.0 0.3 0.5 1.1 1.3 1.5 1.7 1.9 0.9 Current (A)

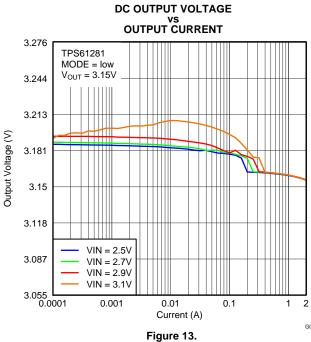
Figure 10.

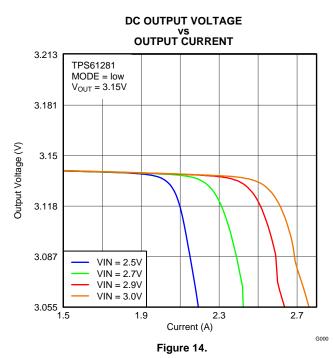


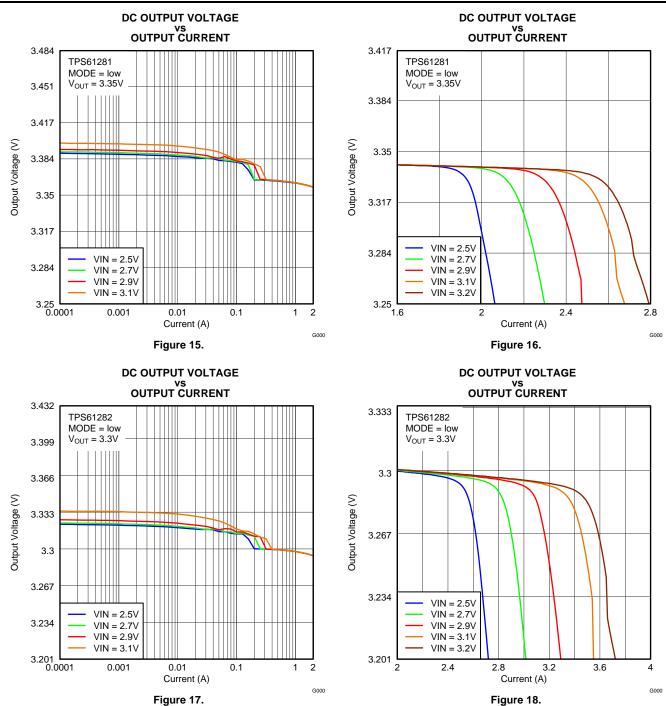
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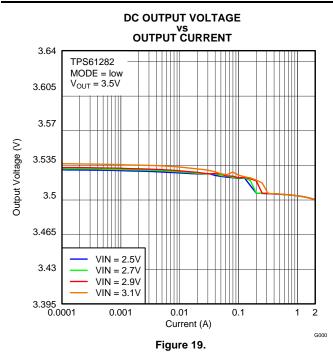


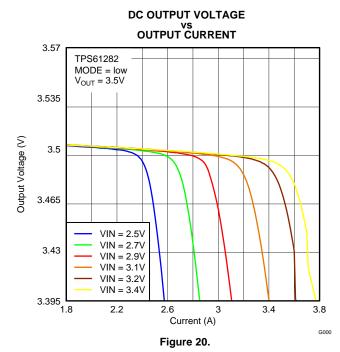


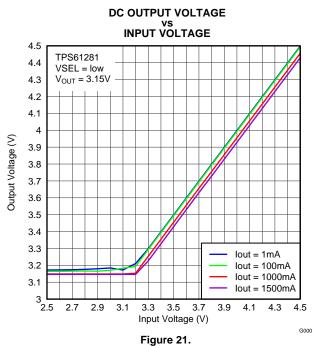


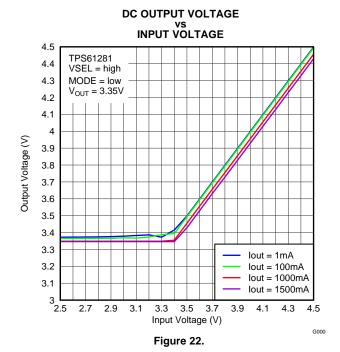


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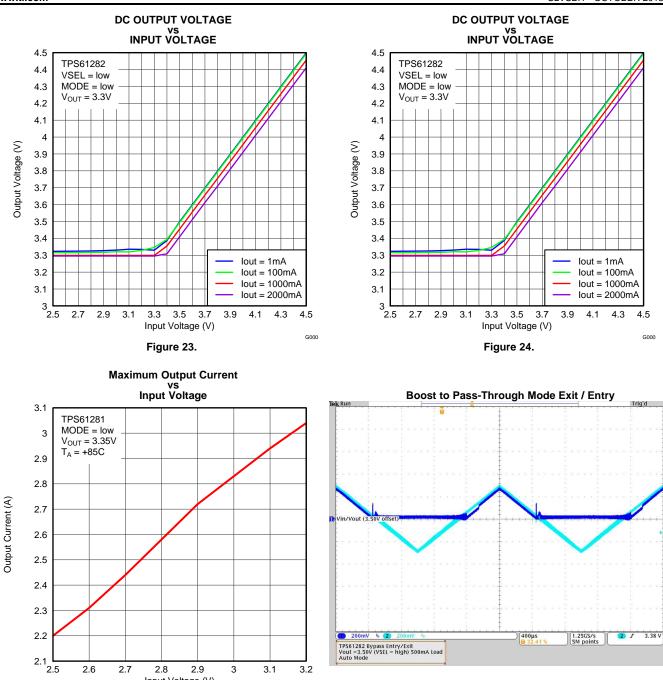


Figure 26.

2.6

2.7

2.8

Input Voltage (V)

Figure 25.

2.9

3.1

3.2

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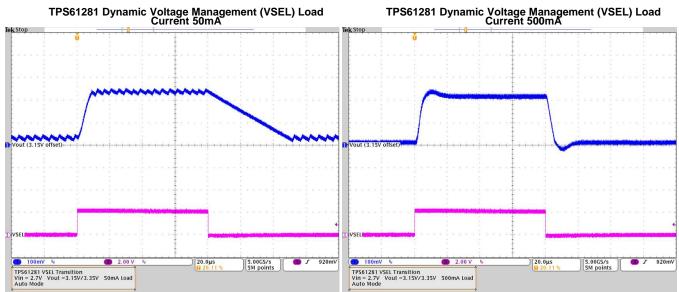


Figure 27. Figure 28.

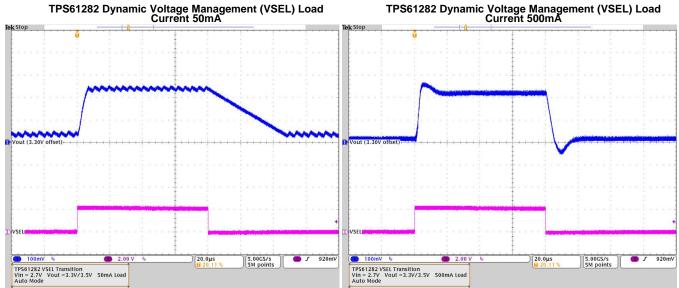


Figure 29. Figure 30.

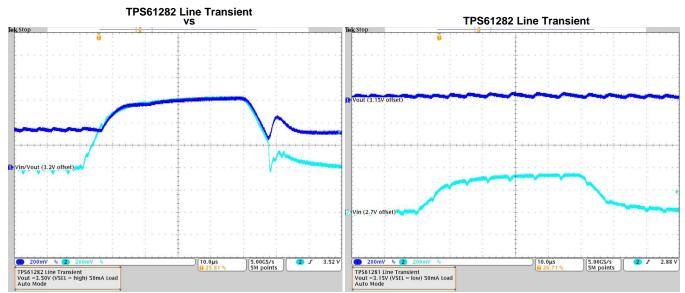


Figure 31. Figure 32.

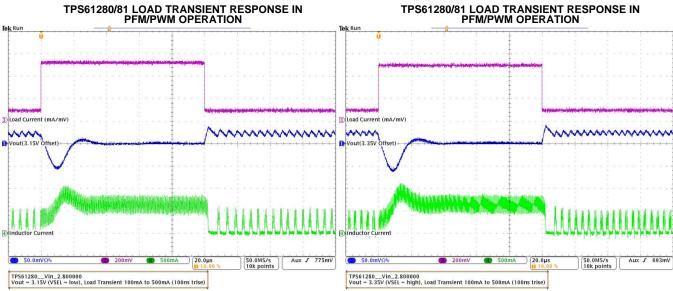


Figure 33. Figure 34.

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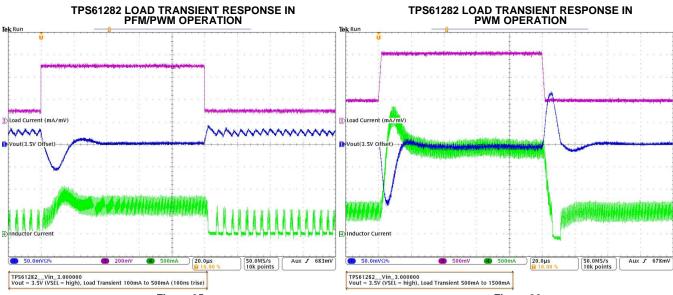


Figure 35. Figure 36.

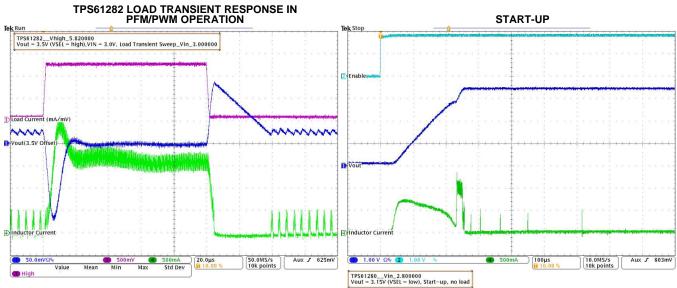


Figure 37. Figure 38.

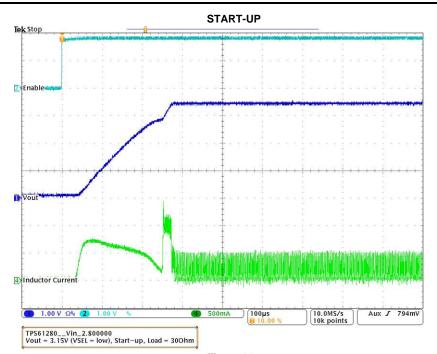


Figure 39.



#### **DETAILED DESCRIPTION**

#### **OPERATION**

The TPS6128x is a high-efficiency step-up converter featuring pass-through mode optimized to provide low-noise voltage supply for 2G RF power amplifiers (PAs) in mobile phones and/or to pre-regulate voltage for supplying subsystem like eMMC memory, audio codec, LCD bias, antenna switches, RF engine PMIC etc... It is designed to allow the system to operate at maximum efficiency for a wide range of power consumption levels from a low-, wide- voltage battery cell.

The capability of the TPS6128x to step-up the voltage as well as to pass-through the input battery voltage when its level is high enough allow systems to operate at maximum performance over a wide range of battery voltages, thereby extending the battery life between charging. The device also addresses brownouts caused by the peak currents drawn by the APU and GPU which can cause the battery rail to droop momentarily. Using the TPS6128x device as a pre-regulator eliminates system brownout condition while maintaining a stable supply rail for critical sub-system to function properly.

The TPS6128x synchronous step-up converter typically operates at a quasi-constant 2.3-MHz frequency pulse width modulation (PWM) at moderate to heavy load currents. At light load currents, the TPS6128x converter operates in power-save mode with pulse frequency modulation (PFM).

In general, a dc/dc step-up converter can only operate in "true" boost mode, i.e. the output "boosted" by a certain amount above the input voltage. The TPS6128x device operates differently as it can smoothly transition in and out of zero duty cycle operation. Depending upon the input voltage, output voltage threshold and load current, the integrated bypass switch automatically transitions the converter into pass-through mode to maintain low-dropout and high-efficiency. The device exits pass-through mode (0% duty cycle operation) if the total dropout resistance in bypass mode is insufficient to maintain the output voltage at it's nominal level. Refer to the typical characteristics section (DC Output Voltage vs. Input Voltage) for further details.

During PWM operation, the converter uses a novel quasi-constant on-time valley current mode control scheme to achieve excellent line/load regulation and allows the use of a small ceramic inductor and capacitors. Based on the  $V_{\text{IN}}/V_{\text{OUT}}$  ratio, a simple circuit predicts the required on-time. At the beginning of the switching cycle, the low-side N-MOS switch is turned-on and the inductor current ramps up to a peak current that is defined by the on-time and the inductance. In the second phase, once the on-timer has expired, the rectifier is turned-on and the inductor current decays to a preset valley current threshold. Finally, the switching cycle repeats by setting the on timer again and activating the low-side N-MOS switch.

The current mode architecture provides excellent transient load response, requiring minimal output filtering. Internal soft-start and loop compensation simplifies the design process while minimizing the number of external components.

The TPS6128x directly and accurately controls the average input current through intelligent adjustment of the valley current limit, allowing an accuracy of ±17.5%. Together with an external bulk capacitor, the TPS6268x allows an application to be interfaced directly to its load, without overloading the input source due to appropriate set average input current limit. An open-drain output (PG or GPIO/nFAULT) provides a signal to issue an interrupt to the system if any fault is detected on the device (thermal shutdown, output voltage out-of limits etc...).

The output voltage can be dynamically adjusted between two values (floor and roof voltages) by toggling a logic control input (VSEL) without the need for external feedback resistors. This features can either be used to raise the output voltage in anticipation of a positive load transient or to dynamically change the PA supply voltage depending on its mode of operation and/or transmitting power.

The TPS61280 integrates an I<sup>2</sup>C compatible interface allowing transfers up to 3.4Mbps. This communication interface can be used to set the output voltage threshold at which the converter transitions between boost and pass-through mode, for reprogramming the mode of operation (PFM/PWM or forced PWM), for settings the average input current limit or resetting the output voltage for instance.

Configuration parameters can be changed by writing the desired values to the appropriate I<sup>2</sup>C register(s). The I<sup>2</sup>C registers are volatile and their contents are lost when power is removed from the device. By writing to the E2PROMCTRL REGISTER, it is possible to store the active configuration in non-volatile E<sup>2</sup>PROM; during power-up, the contents of the E<sup>2</sup>PROM are copied into the I<sup>2</sup>C registers and used to configure the device.

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#### **POWER-SAVE MODE**

The TPS6128x integrates a power-save mode to improve efficiency at light load. In power save mode the converter only operates when the output voltage trips below a set threshold voltage. It ramps up the output voltage with several pulses and goes into power save mode once the output voltage exceeds the set threshold voltage. The PFM mode is left and PWM mode entered in case the output current can not longer be supported in PFM mode.

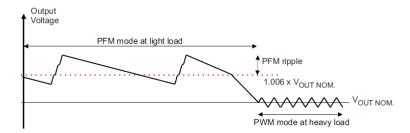


Figure 40. Power-Save Mode Ripple

#### **PASS-THROUGH MODE**

The TPS6128x contains an internal switch for bypassing the dc/dc boost converter during pass-through mode. When the input voltage is larger than the preset output voltage, the converter seamlessly transitions into 0% duty cycle operation and the bypass FET is fully enhanced. Entry in pass-through mode is triggered by condition where  $V_{IN} > V_{OUT}$  and no switching has occurred during past 16µs.

In this mode of operation, the load (2G RF PA for instance) is directly supplied from the battery for maximum RF output power, highest efficiency and lowest possible input-to-output voltage difference. The device consumes only a standby current of 15µA (typ). In pass-through mode, the device is short-circuit protected by a very fast current limit detection scheme.

During this operation, the output voltage follows the input voltage and will not fall below the programmed output voltage threshold as the input voltage decreases. The output voltage drop during pass-through mode depends on the load current and input voltage, the resulting output voltage is calculated as:

$$V_{OUT} = V_{IN} - (R_{DSON(BP)} \bullet I_{OUT})$$
(1)

Conversely, the efficiency in pass-through mode is defined as:

$$\eta = 1 - R_{\text{DSON(BP)}} \frac{I_{\text{OUT}}}{V_{\text{IN}}}$$
(2)

in which R<sub>DSON(BP)</sub> is the typical on-resistance of the bypass FET

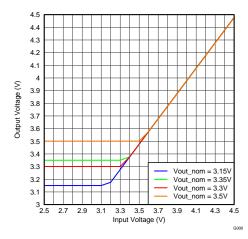


Figure 41. DC Output Voltage vs. Input Voltage

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Pass-through mode exit is triggered when the output voltage reaches the pre-defined threshold (e.g. 3.4V).

During pass-through mode, the TPS6128x device is short-circuit protected by a very fast current limit detection scheme. If the current in the pass-through FET exceeds approximately 7.3Amps a fault is declared and the device cycles through a start-up procedure.

#### **MODE SELECTION**

Depending on the settings of CONFIG REGISTER the device can be operated at a guasi-constant 2.3-MHz frequency PWM mode or in automatic PFM/PWM mode. In this mode, the converter operates in pseudo-fixed frequency PWM mode at moderate to heavy loads and in the PFM mode during light loads, which maintains high efficiency over a wide load current range. For more details, see the CONFIG REGISTER description.

The quasi-constant frequency PWM mode has the tightest regulation and the best line/load transient performance. In forced PWM mode, the device features a unique R<sub>DS(ON)</sub> management function to maintain high broadband efficiency as well as low resistance in pass-through mode.

In the TPS61280 device, the GPIO pin can be configured (via the CONFIG REGISTER) to select the operating mode of the device. In the other TPS6128x devices, the MODE pin is used to select the operating mode. Pulling this pin high forces the converter to operate in the PWM mode even at light load currents. The advantage is that the converter modulates its switching frequency according to a spread spectrum PWM modulation technique allowing simple filtering of the switching harmonics in noise-sensitive applications.

For additional flexibility, it is possible to switch from power-save mode (GPIO or MODE input = L) to PWM mode (GPIO or MODE input = H) during operation. This allows efficient power management by adjusting the operation of the converter to the specific system requirements (e.g. 2G RF PA Rx/Tx operation).

#### **NOTE**

During start-up (conventionally or when recovering from thermal shutdown) the device must be set to operate with auto PFM/PWM mode. Consequently, the device determines automatically PFM or PWM mode depending on the output's load. Once the output voltage settled and PG pin indicates that the converter's output voltage is within its regulation limits, the device can be forced in PWM mode operation, if desired.

Entry to forced pass-through mode (nBYP = L) initiates with a current limited transition followed by a true bypass state. To prevent reverse current to the battery, the devices waits until the output discharges below the input voltage level before entering forced pass-through mode. Care should be taken to prohibit the output voltage from collapsing whilst transitioning into forced pass-through mode under heavy load conditions and/or limited output capacitance. This can be easily done by adding capacitance to the output of the converter. In forced passthrough mode, the output follows the input below the preset output threshold voltage (VOUT\_TH).

#### **VOLTAGE SCALING MANAGEMENT (VSEL)**

In order to maintain a certain minimum output voltage under heavy load transients, the output voltage set point can be dynamically increased by asserting the VSEL input. The functionality also helps to mitigate undershoot during severe line transients, while minimizing the output voltage during more benign operating conditions to save power.

The output voltage ramps up (floor to roof transition) at pre-defined rate defined by the average input current limit setting. The required time to ramp down the voltage (roof to floor transition) largely depends on the amount of capacitance present at the converter's output as well as on the load current. Table 4 shows the ramp rate control when transitioning to a lower voltage.

#### Table 4. Ramp Down Rate vs. Target Mode

Mode Associated with Floor Voltage	Output Voltage Ramp Rate
Forced PWM	Output capacitance is being discharged at a rate of approx. 50mA (or higher) constant current in addition to the load current drawn
PFM	Output capacitance is being discharged (solely) by the load current drawn

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#### SPREAD SPECTRUM, PWM FREQUENCY DITHERING

The goal is to spread out the emitted RF energy over a larger frequency range so that the resulting EMI is similar to white noise. The end result is a spectrum that is continuous and lower in peak amplitude, making it easier to comply with electromagnetic interference (EMI) standards and with the power supply ripple requirements in cellular and non-cellular wireless applications. Radio receivers are typically susceptible to narrowband noise that is focused on specific frequencies.

Switching regulators can be particularly troublesome in applications where electromagnetic interference (EMI) is a concern. Switching regulators operate on a cycle-by-cycle basis to transfer power to an output. In most cases, the frequency of operation is either fixed or regulated, based on the output load. This method of conversion creates large components of noise at the frequency of operation (fundamental) and multiples of the operating frequency (harmonics).

The spread spectrum architecture varies the switching frequency by ca.  $\pm 15\%$  of the nominal switching frequency thereby significantly reducing the peak radiated and conducting noise on both the input and output supplies. The frequency dithering scheme is modulated with a triangle profile and a modulation frequency  $f_m$ .

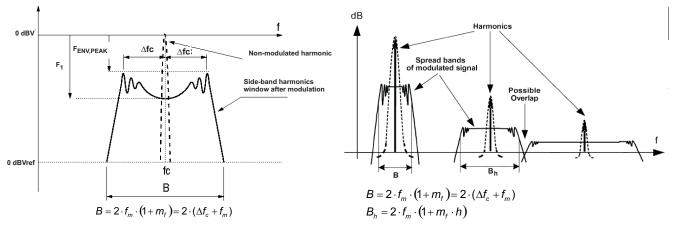


Figure 42. Spectrum of a Frequency Modulated Sin. Wave with Sinusoidal Variation in Time

Figure 43. Spread Bands of Harmonics in Modulated Square Signals (1)

The above figures show that after modulation the sideband harmonic is attenuated compared to the non-modulated harmonic, and the harmonic energy is spread into a certain frequency band. The higher the modulation index (*mf*) the larger the attenuation.

$$\mathsf{m}_f = \frac{\delta \times f_{\mathrm{c}}}{f_{\mathrm{m}}} \tag{3}$$

With:

 $f_c$  is the carrier frequency (approx. 2.3MHz)

 $f_m$  is the modulating frequency (approx. 40kHz)

 $\delta$  is the modulation ratio (approx 0.15)

$$\delta = \frac{\Delta f_{\rm c}}{f_{\rm c}} \tag{4}$$

The maximum switching frequency  $f_c$  is limited by the process and finally the parameter modulation ratio ( $\delta$ ), together with  $f_m$ , which is the side-band harmonics bandwidth around the carrier frequency  $f_c$ . The bandwidth of a frequency modulated waveform is approximately given by the Carson's rule and can be summarized as:

$$B = 2 \times f_{m} \times (1 + m_{f}) = 2 \times (\Delta f_{c} + f_{m})$$
(5)

 Spectrum illustrations and formulae (Figure 42 and Figure 43) copyright IEEE TRANSACTIONS ON ELECTROMAGNETIC COMPATIBILITY, VOL. 47, NO.3, AUGUST 2005.



 $f_m$  < RBW: The receiver is not able to distinguish individual side-band harmonics, so, several harmonics are added in the input filter and the measured value is higher than expected in theoretical calculations.

 $f_m$  > RBW: The receiver is able to properly measure each individual side-band harmonic separately, so the measurements match with the theoretical calculations.

#### **CURRENT LIMIT OPERATION**

The TPS6128x device features a valley inductor current limit scheme.

In dc/dc boost mode, the TPS6128x device employs a current limit detection scheme in which the voltage drop across the synchronous rectifier is sensed during the off-time. In the TPS61280 the current limit threshold can be set via an I<sup>2</sup>C register. TPS6128x devices have a fixed current limit threshold. See device ordering table for detailed information.

The output voltage is reduced as the power stage of the device operates in a constant current mode. The maximum continuous output current (I<sub>OUT(MAX)</sub>), before entering current limit (CL) operation, can be defined by Equation 6.

$$I_{OUT(MAX)} = I_{LIM} \cdot \frac{V_{IN}}{V_{OUT}} \cdot \eta$$
(6)

The inductor peak-to-peak current ripple ( $\Delta I_1$ ) is calculated by Equation 7

$$\Delta I_{L} = \frac{V_{IN}}{L} \cdot \frac{D}{f} \tag{7}$$

The output current, I<sub>OUT(DC)</sub>, is the average of the rectifier ripple current waveform. When the load current is increased such that the trough is above the current limit threshold, the off-time is increased to allow the current to decrease to this threshold before the next on-time begins (so called frequency fold-back mechanism). When the current limit is reached the output voltage decreases during further load increase.

Figure 44 illustrates the inductor and rectifier current waveforms during current limit operation.

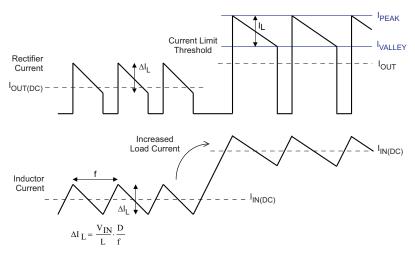


Figure 44. Inductor/Rectifier Currents in Current Limit Operation (DC/DC Boost Mode)

During pass-through mode, the TPS6128x device is short-circuit protected by a very fast current limit detection scheme. If the current in the bypass FET exceeds approximately 7.5Amps a fault is declared and the device cycles through a start-up procedure.

28 Subm

#### START-UP AND SHUTDOWN MODE

The TPS6128x automatically powers-up as soon as the input voltage is applied. The device has an internal softstart circuit that limits the inrush current during start-up. The first phase in the start-up procedure is to bias the output node close to the input level (so called pre-charge phase).

In this operating mode, the device limits its output current to ca. 500mA. Should the output voltage not have reached the input level within a maximum duration of 750µs, the device automatically increases its pre-charge current to ca. 2000mA ( $ILIM[3:0] \ge 1000$ ) or maintains it around 500mA ( $ILIM[3:0] \le 0111$ ). If the output voltage still fails to reach its target after 1.5ms ( $ILIM[3:0] \ge 1000$ ) or 50ms ( $ILIM[3:0] \le 0111$ ), a fault condition is declared. After waiting 1ms, a restart is attempted.

During start-up, it is recommended to keep DC load current draw below 250mA.

The TPS6128x device contains a thermal regulation loop that monitors the die temperature during the pre-charge phase. If the die temperature rises to high values of about 110°C, the device automatically reduces the current to prevent the die temperature from increasing further. Once the die temperature drops about 10°C below the threshold, the device will automatically increase the current to the target value. This function also reduces the current during a short-circuit condition.

When the EN and nBYP pins are set high, the device enters normal operation (i.e. automatic dc/dc boost, pass-through mode) and ensures that the output voltage remains above a pre-defined threshold (e.g. 3.3V).

Setting the EN pin low (nBYP = 1) forces the TPS6128x device in shutdown mode with a current consumption of <8.5µA typ. In this mode, the output of the converter is regulated to a minimum level so as to limit the input-to-output voltage difference to less than 3.6V (typ). The device is capable of sinking up to 10mA output current and prohibits reverse current flow from the output to the input. For proper operation, the EN pin must be terminated and must not be left floating.

Changing operating mode from auto mode (EN = nBYP = 1) to low  $I_Q$  Pass-through mode (EN = nBYP = 0) with device pins EN and nBYP can either be done controlling EN and nBYP pins from same control signal (delay between signal < 60ns) or first switching in forced pass-through mode (EN = 1, nBYP = 0) followed by switching to low  $I_Q$  Pass-through mode (EN = nBYP = 0).

The TPS6128x device also features the possibility of shutting the converter's output for a short period of time, either via the nRST/nFAULT (GPIO). Pulling this input low initiates a reset of the converter's output. The sequence is falling edge-triggered and consists of a discharge phase (down to ca. 600mV or lower) of the capacitance located at the converter's output followed by a start-up phase.

EN Input	nBYP Input	Device State
0	0	The device is shut down in pass-through mode featuring a shutdown current down to ca. 2µA typ. The load current capability is limited (up to ca. 250mA).
0	1	The device is shut down and the output voltage is reduced to a minimum value (VIN - VOUT $\leq$ 3.6V). The device shutdown current is approximately 8.5 $\mu$ A typ.
1	0	The device is active in forced pass-through mode. The device supply current is approximately 15µA typ. from the battery. The device is short circuit protected by a current limit of ca.7300mA.
1	1	The device is active in auto mode (dc/dc boost, pass-through). The device supply current is approximately 50µA typ. from the battery.

Table 5. Mode of Operation

### **UNDERVOLTAGE LOCKOUT**

The under voltage lockout circuit prevents the device from malfunctioning at low input voltages and the battery from excessive discharge. The I2C control interface and the output stage of the converter are disabled once the falling  $V_{IN}$  trips the under-voltage lockout threshold  $V_{UVLO}$  (2.0V typ). The device starts operation once the rising  $V_{IN}$  trips  $V_{UVLO}$  threshold plus its hysteresis of 100 mV at typ. 2.1V.

#### THERMAL SHUTDOWN

As soon as the junction temperature, T<sub>J</sub>, exceeds 150°C (typ.) the device goes into thermal shutdown. In this mode the bypass, high-side and low-side MOSFETs are turned-off. When the junction temperature falls below the thermal shutdown minus its hysteresis, the device continuous the operation.

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The TPS6128x enters the fault state under any of the followings conditions:

- The output voltage fails to achieve the required level during a start-up phase.
- The output voltage falls out of regulation (in pre-charge mode).
- The device has entered thermal shutdown.

Once a fault is triggered, the regulator stops operating and disconnects the load. After waiting 1ms, the device attempts to restart. The TPS61280 device can be configured to signal a fault condition by pulling the open-drain GPIO pin (nFAULT) low for a short period of time. The nFAULT output provides a falling edge triggered interrupt signal to the host. To ensure proper operation, the GPIO port needs to be pull high quick enough, i.e. faster than ca. 200ns. To do so, it is recommended to use a GPIO pull-up resistor in the range of  $1k\Omega$  to  $10k\Omega$ .

The TPS6128x (simple logic I/F version) device only provide a power-good output (PG) for signaling the system when the regulator has successfully completed start-up and no faults have occurred. Power-good also functions as an early warning flag for excessive die temperature and overload conditions.

- PG is asserted high when the start-up sequence is successfully completed.
- PG is pulled low when the output voltage falls approx. 10% below its regulation level or the die temperature exceeds 115°C. PG is re-asserted high when the device cools below ca. 100°C.
- Any fault condition causes PG to be de-asserted.
- PG is pulled high when the device is operating in forced pass-through mode (i.e. nBYP = L).
- PG is pulled high when the device is in shutdown mode.

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#### **SERIAL INTERFACE DESCRIPTION (TPS61280)**

I<sup>2</sup>C<sup>TM</sup> is a 2-wire serial interface developed by Philips Semiconductor, now NXP Semiconductors (see I2C-Bus Specification, Version 2.1, January 2000). The bus consists of a data line (SDA) and a clock line (SCL) with pull-up structures. When the bus is *idle*, both SDA and SCL lines are pulled high. All the I<sup>2</sup>C compatible devices connect to the I<sup>2</sup>C bus through open drain I/O pins, SDA and SCL. A *master* device, usually a microcontroller or a digital signal processor, controls the bus. The master is responsible for generating the SCL signal and device addresses. The master also generates specific conditions that indicate the START and STOP of data transfer. A *slave* device receives and/or transmits data on the bus under control of the master device.

The TPS6128x device works as a *slave* and supports the following data transfer *modes*, as defined in the I<sup>2</sup>C-Bus Specification: standard mode (100 kbps) and fast mode (400 kbps), fast mode plus (1 Mbps) and high-speed mode (3.4 Mbps). The interface adds flexibility to the power supply solution, enabling most functions to be programmed to new values depending on the instantaneous application requirements. Register contents remain intact as long as supply voltage remains above 2.1V.

The data transfer protocol for standard and fast modes is exactly the same, therefore they are referred to as F/S-mode in this document. The protocol for high-speed mode is different from F/S-mode, and it is referred to as HS-mode. The TPS6128x device supports 7-bit addressing; 10-bit addressing and general call address are not supported. The device 7bit address is defined as '111 0101'.

It is recommended that the I2C masters initiates a STOP condition on the I2C bus after the initial power up of SDA and SCL pull-up voltages to ensure reset of the TPS6128x I2C engine.

#### STANDARD-, FAST-, FAST-MODE PLUS PROTOCOL

The master initiates data transfer by generating a start condition. The start condition is when a high-to-low transition occurs on the SDA line while SCL is high, as shown in Figure 45. All I<sup>2</sup>C-compatible devices should recognize a start condition.

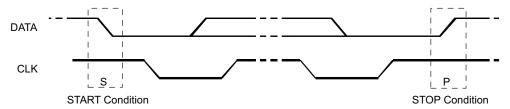


Figure 45. START and STOP Conditions

The master then generates the SCL pulses, and transmits the 7-bit address and the read/write direction bit R/W on the SDA line. During all transmissions, the master ensures that data is valid. A valid data condition requires the SDA line to be stable during the entire high period of the clock pulse (see Figure 46). All devices recognize the address sent by the master and compare it to their internal fixed addresses. Only the slave device with a matching address generates an acknowledge (see Figure 47) by pulling the SDA line low during the entire high period of the ninth SCL cycle. Upon detecting this acknowledge, the master knows that communication link with a slave has been established.

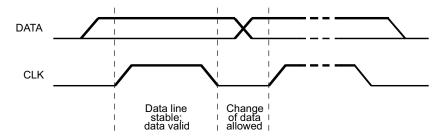


Figure 46. Bit Transfer on the Serial Interface

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The master generates further SCL cycles to either transmit data to the slave (R/W bit 1) or receive data from the slave (R/W bit 0). In either case, the receiver needs to acknowledge the data sent by the transmitter. So an acknowledge signal can either be generated by the master or by the slave, depending on which one is the receiver. 9-bit valid data sequences consisting of 8-bit data and 1-bit acknowledge can continue as long as necessary.

To signal the end of the data transfer, the master generates a stop condition by pulling the SDA line from low to high while the SCL line is high (see Figure 45). This releases the bus and stops the communication link with the addressed slave. All I<sup>2</sup>C compatible devices must recognize the stop condition. Upon the receipt of a stop condition, all devices know that the bus is released, and they wait for a start condition followed by a matching address.

Attempting to read data from register addresses not listed in this section will result in 00h being read out.

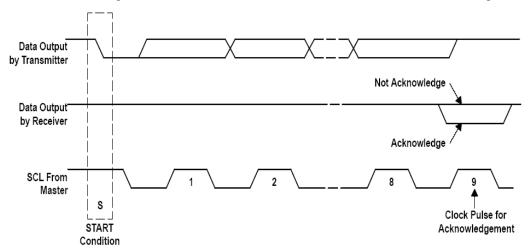


Figure 47. Acknowledge on the I<sup>2</sup>C Bus

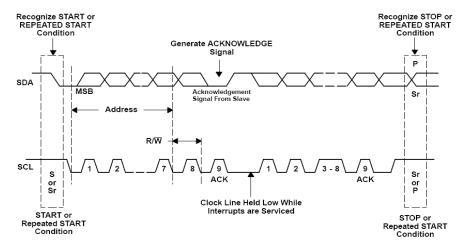


Figure 48. Bus Protocol

#### **HS-MODE PROTOCOL**

The master generates a start condition followed by a valid serial byte containing HS master code 00001XXX. This transmission is made in F/S-mode at no more than 400 Kbps. No device is allowed to acknowledge the HS master code, but all devices must recognize it and switch their internal setting to support 3.4 Mbps operation.

2 S

The master then generates a *repeated start condition* (a repeated start condition has the same timing as the start condition). After this repeated start condition, the protocol is the same as F/S-mode, except that transmission speeds up to 3.4 Mbps are allowed. A stop condition ends the HS-mode and switches all the internal settings of the slave devices to support the F/S-mode. Instead of using a stop condition, repeated start conditions should be used to secure the bus in HS-mode.

Attempting to read data from register addresses not listed in this section will result in 00h being read out.

#### TPS6128x I<sup>2</sup>C UPDATE SEQUENCE

The TPS6128x requires a start condition, a valid I<sup>2</sup>C address, a register address byte, and a data byte for a single update. After the receipt of each byte, TPS6128x device acknowledges by pulling the SDA line low during the high period of a single clock pulse. A valid I<sup>2</sup>C address selects the TPS6128x. TPS6128x performs an update on the falling edge of the acknowledge signal that follows the LSB byte.

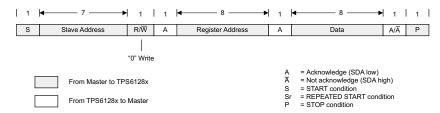


Figure 49. : "Write" Data Transfer Format in Standard-, Fast, Fast-Plus Modes

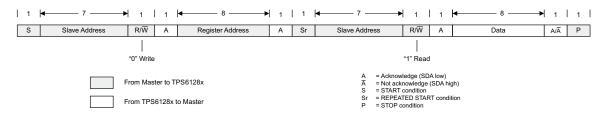


Figure 50. "Read" Data Transfer Format in Standard-, Fast, Fast-Plus Modes

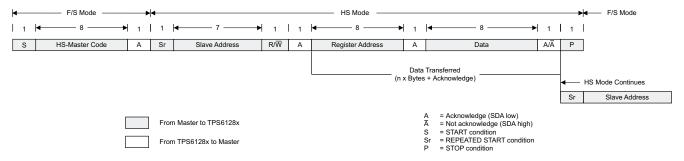


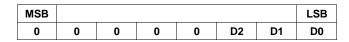
Figure 51. Data Transfer Format in H/S-Mode

#### **SLAVE ADDRESS BYTE**

MSB						LSB
1	1	1	0	1	<b>A</b> 1	A0

The slave address byte is the first byte received following the START condition from the master device.

#### **REGISTER ADDRESS BYTE**



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Following the successful acknowledgment of the slave address, the bus master will send a byte to the TPS6128x, which will contain the address of the register to be accessed.

## I<sup>2</sup>C REGISTERS, E<sup>2</sup>PROM, WRITE PROTECT

Configuration parameters can be changed by writing the desired values to the appropriate I<sup>2</sup>C register(s). The I<sup>2</sup>C registers are volatile and their contents are lost when power is removed from the device. By writing to the E2PROMCTRL REGISTER, it is possible to store the active configuration in non-volatile E<sup>2</sup>PROM; during power-up, the contents of the E<sup>2</sup>PROM are copied into the I<sup>2</sup>C registers and used to configure the device.

#### NOTE

An active high Write Protect (WP) bit prevents the configuration parameters from being changed by accident. Once the E<sup>2</sup>PROM memory has been programmed with Write Protect (WP) bit set, its content will be locked and can not be reprogrammed any more.

Configuration parameters can be read from the I<sup>2</sup>C register(s) or E<sup>2</sup>PROM registers at any time (the WP bit has no effect on read operations).

#### E<sup>2</sup>PROM CONFIGURATION PARAMETERS

Table 6 shows the memory map of the configuration parameters.

rable of Comigaration memory map					
Register Address	Register Name	Factory Default	Description		
01h	CONFIG REGISTER	xxh	Sets miscellaneous configuration bits		
02h	VOUTFLOORSET REGISTER	xxh	Sets the floor output voltage threshold boost / pass-through mode change $(VSEL = L)$		
03h	VOUTROOFSET REGISTER	xxh	Sets the roof output voltage threshold boost / pass-through mode change (VSEL = H)		
04h	ILIMSET REGISTER	xxh	Sets the average input current limit in dc/dc boost mode		
05h	STATUS REGISTER	xxh	Returns status flags		
FFh	E2PROMCTRL REGISTER	00h	Controls whether read and write operations access I <sup>2</sup> C or E <sup>2</sup> PROM registers		

**Table 6. Configuration Memory Map** 

The below procedure details how to save the content of all  $I^2C$  registers to the  $E^2PROM$  non-volatile configuration memory.

- 1. Bus master sends START condition
- 2. Bus master sends 7-bit slave address plus low R/W bit (for example EAh)
- 3. TPS6128x acknowledges (SDA low)
- 4. Bus master sends address of E2PROMCTRL REGISTER (FFh)
- TPS6128x acknowledges (SDA low)
- 6. Bus master sends data to be written to the Control Register (C0h)
- 7. TPS6128x acknowledges (SDA low)
- 8. Bus master sends STOP condition



Figure 52. Saving Contents of all I<sup>2</sup>C Registers to E<sup>2</sup>PROM

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# **VERSION REGISTER**

Memory location: 0x00

Description		SILICON REVISION						
Bits	D7	D6	D5	D4	D3	D2	D1	D0
Memory type	R	R	R	R	R	R	R	R
Default value	X	X	X	X	X	X	X	X
Stored in E <sup>2</sup> PROM?	N	N	N	N	N	N	N	N

Bit	Description
SILICON REVISION [7:0]	Silicon revision bits.
	00000000: PG1.0 silicon
	0000001: PG1.1 silicon 00000010: PG1.2 silicon

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#### **CONFIG REGISTER**

Memory location: 0x01

Description	RESET	ENABLE		RESERVED	GPIOCFG	SSFM	MODE_CTRL	
Bits	D7	D6	D5	D4	D3	D2	D1	D0
Memory type	R/W	R/W	R/W	R/W	R/W	R/W	R/W	R/W
Default value	0	0	0	0	0	0	0	1
Stored in E <sup>2</sup> PROM?	N	Y	Υ	Z	Υ	Y	Y	Υ

Bit	Description					
RESET	Device reset bit.  0: Normal operation.  1: Default values are set to all internal registers. The device operation is cycled (ON-OFF-ON), i.e. the converter is disabled for a short period of time and the output is reset.					
ENABLE[1:0]	Device enable bits.  00: Device operation follows hardware control signal (refer toTable 5).  01: Device operates in auto transition mode (dc/dc boost, bypass) regardless of the nBYP control signal (EN = 1).  10: Device is forced in pass-through mode regardless of the nBYP control signal (EN = 1).  11: Device is in shutdown mode. The output voltage is reduced to a minimum value (VIN - VOUT ≤ 3.6V) regardless of the nBYP control signal (EN = 1).					
RESERVED	Reserved bit.  This bits is reserved for future use. During write operations data intended for this bit is ignored, and during read operations 0 is returned.					
GPIOCFG	<ul><li>GPIO port configuration bit.</li><li>0: GPIO port is configured to support manual reset input (nRST) and interrupt generation output (nFAULT).</li><li>1: GPIO port is configured as a device mode selection input.</li></ul>					
SSFM	Spread modulation control.  0: Spread spectrum modulation is disabled.  1: Spread spectrum modulation is enabled in PWM mode.					
MODE_CTRL[1:0]	Device mode of operation bits.  00: Device operation follows hardware control signal (GPIO must be configured as mode selection input).  01: PFM with automatic transition into PWM operation.  10: Forced PWM operation.  11: PFM with automatic transition into PWM operation (VSEL = L), forced PWM operation (VSEL = H).					
	NOTE  During start-up the device must be set to operate with auto PFM/PWM mode. Consequently, the device determines automatically PFM or PWM mode depending on the output's load. Once the output voltage settled and PG pin indicates that the converter's output voltage is within its regulation limits, the device can be forced in PWM mode operation, if desired.					

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# **VOUTFLOORSET REGISTER**

Memory location: 0x02

Description	RESERVED	RESERVED	RESERVED	VOUTFLOOR_TH						
Bits	D7	D6	D5	D4	D3	D2	D1	D0		
Memory type	R/W	R/W	R/W	R/W	R/W	R/W	R/W	R/W		
Default value	0	0	0	0	0	1	1	0		
Stored in E <sup>2</sup> PROM?	N	N	N	Y	Y	Y	Y	Y		

Bit	Description								
RESERVED	Reserved bit.								
	This bits is reserved for future use. During write operations data intended for this bit is ignored, and during read operations 0 is returned.								
VOUTFLOOR_TH[4:0]									
	11101: 4.300V 11110: 4.350V								
	11111: 4.400V								

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# **VOUTROOFSET REGISTER**

Memory location: 0x03

Description	RESERVED	RESERVED	RESERVED	VOUTROOF_TH						
Bits	D7	D6	D5	D4	D3	D2	D1	D0		
Memory type	R/W	R/W	R/W	R/W	R/W	R/W	R/W	R/W		
Default value	0	0	0	0	1	0	1	0		
Stored in E <sup>2</sup> PROM?	N	N	N	Υ	Y	Y	Y	Y		

Bit	Description								
RESERVED	Reserved bit.								
	This bits is reserved for future use. During write operations data intended for this bit is ignored, and during read operations 0 is returned.								
VOUTROOF_TH[4:0]	Output voltage threshold, dc/dc boost / pass-through mode change.								
	00000: 2.850V								
	00001: 2.900V								
	00010: 2.950V								
	00011: 3.000V								
	00100: 3.050V								
	00101: 3.100V								
	00110: 3.150V								
	00111: 3.200V								
	01000: 3.250V								
	01001: 3.300V								
	01010: 3.350V								
	01011: 3.400V								
	01100: 3.450V								
	01101: 3.500V								
	01110: 3.550V								
	01111: 3.600V								
	10000: 3.650V								
	10001: 3.700V								
	10010: 3.750V								
	10011: 3.800V								
	10100: 3.850V								
	10101: 3.900V								
	10110: 3.950V								
	10111: 4.000V								
	11000: 4.050V								
	11001: 4.100V								
	11010: 4.150V								
	11011: 4.200V 11100: 4.250V								
	11100: 4.250V 11101: 4.300V								
	1110: 4.350V 11110: 4.350V								
	11111: 4.400V								

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### **ILIMSET REGISTER**

Memory location: 0x04

Description	RESERVED	RESERVED	ILIM OFF	Soft-start	ILIM				
Bits	D7	D6	D5	D4	D3	D2	D1	D0	
Memory type	R/W	R/W	R/W	R/W	R/W	R/W	R/W	R/W	
Default value	0	0	0	1	1	0	1	1	
Stored in E <sup>2</sup> PROM?	N	N	N	Y	Y	Y	Y	Y	

Bit	Description								
RESERVED	Reserved bit.  This bits is reserved for future use. During write operations data intended for this bit is ignored, and during read operations 0 is returned.								
ILIM[3:0]	Inductor valley current limit in dc/dc boost mode (COUTRNG bit = 0) <sup>(1)</sup> .  1000: 1500mA  1001: 2000mA  1010: 2500mA  1011: 3000mA  1100: 3500mA  1101: 4000mA  1110: 4500mA  1111: 5000mA								
Soft-Start	Soft-start selection bit. 0: DC/DC boost soft-start current is limited per ILIM bit settings 1: DC/DC boost soft-start current is limited to ca. 1250mA inductor valley current								
ILIM OFF	Enable/Disable Current Limit 0 : Current Limit Enabled 1 : Current Limit Disabled								

<sup>(1)</sup> Refer to START-UP AND SHUTDOWN MODE section for additional information.

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## **STATUS REGISTER**

Memory location: 0x05

Description	TSD	HOTDIE	DCDCMODE	OPMODE	ILIMPT	ILIMBST	FAULT	PGOOD
Bits	D7	D6	D5	D4	D3	D2	D1	D0
Memory type	R	R	R	R	R	R	R	R
Default value	0	0	0	0	0	0	0	0
Stored in E <sup>2</sup> PROM?	N	N	Z	N	N	N	N	N

Bit	Description
TSD	Thermal shutdown status bit. 0: Normal operation. 1: Thermal shutdown tripped. This flag is reset after readout.
HOTDIE	Instantaneous die temperature bit. 0: $T_J < 115^{\circ}C$ . 1: $T_J > 115^{\circ}C$ .
DCDCMODE	DC/DC mode of operation status bit. 0: Device operates in PFM mode. 1: Device operates in PWM mode.
OPMODE	Device mode of operation status bit.  0: Device operates in pass-through mode.  1: Device operates in dc/dc mode.
ILIMPT	Current limit status bit (pass-through mode). 0: Normal operation. 1: Indicates that the bypass FET current limit has triggered. This flag is reset after readout.
ILIMBST	Current limit status bit (dc/dc boost mode).  0: Normal operation.  1: Indicates that the average input current limit has triggered for 1.5ms in dc/dc boost mode. This flag is reset after readout.
FAULT	<ul><li>FAULT status bit.</li><li>0: Normal operation.</li><li>1: Indicates that a fault condition has occurred. This flag is reset after readout.</li></ul>
PGOOD	Power Good status bit. 0: Indicates the output voltage is out of regulation. 1: Indicates the output voltage is within its nominal range. This bit is set if the converter is forced in pass-through mode.

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# **E2PROMCTRL REGISTER**

Memory location: 0xFF

Description	WEN	WP	ISE2PROMWP	RESERVED	RESERVED	RESERVED	RESERVED	RESERVED
Bits	D7	D6	D5	D4	D3	D2	D1	D0
Memory type	R/W	R/W	R	R/W	R/W	R/W	R/W	R/W
Default value	0	0	0	0	0	0	0	0
Stored in E <sup>2</sup> PROM?	N	Υ	N	N	N	N	N	N

Bit	Description								
WEN	E <sup>2</sup> PROM Write Enable bit.								
	0: No operation. 1: Forces the contents of selected I <sup>2</sup> C register bits to be copied into E <sup>2</sup> PROM, thereby making them the default values during power-up. When the contents of all the I <sup>2</sup> C register bits have been written to the E <sup>2</sup> PROM, the device automatically resets this bit.								
WP	E <sup>2</sup> PROM Write Protect bit.  0: Normal operation.  1: Forces the E <sup>2</sup> PROM content to be locked following a write sequence (WEN = 1). This protects the E <sup>2</sup> PROM content from undesirable write actions making it virus safe. This process is non reversible.								
ISE2PROMWP	E <sup>2</sup> PROM Write Protect Status bit.  0: E <sup>2</sup> PROM content is not write protected. E <sup>2</sup> PROM content can still be updated.  1: E <sup>2</sup> PROM content is write protected. E <sup>2</sup> PROM content is permanently locked.								
RESERVED	Reserved bit.  This bits is reserved for future use. During write operations data intended for this bit is ignored, and during read operations 0 is returned.								

**STRUMENTS** 

#### APPLICATION INFORMATION

#### INDUCTOR SELECTION

A boost converter normally requires two main passive components for storing energy during the conversion, an inductor and an output capacitor are required. It is advisable to select an inductor with a saturation current rating higher than the possible peak current flowing through the power switches.

The inductor peak current varies as a function of the load, the input and output voltages and can be estimated using Equation 8.

$$I_{L(PEAK)} = \frac{V_{IN} \cdot D}{2 \cdot f \cdot L} + \frac{I_{OUT}}{(1-D) \cdot \eta} \quad \text{with} \quad D = 1 - \frac{V_{IN}}{V_{OUT}}$$
(8)

Selecting an inductor with insufficient saturation performance can lead to excessive peak current in the converter. This could eventually harm the device and reduce it's reliability.

When selecting the inductor, as well as the inductance, parameters of importance are: maximum current rating, series resistance, and operating temperature. The inductor DC current rating should be greater (by some margin) than the maximum input average current, refer to Equation 9 and CURRENT LIMIT OPERATION section for more details.

$$I_{L(DC)} = \frac{V_{OUT}}{V_{IN}} \cdot \frac{1}{\eta} \cdot I_{OUT}$$
(9)

The TPS6128x series of step-up converters have been optimized to operate with a effective inductance in the range of 200nH to 800nHµH and with output capacitors in the range of 8F to 100µF . The internal compensation is optimized for an output filter of L = 0.5µH and  $C_O$  = 15µF. Larger or smaller inductor values can be used to optimize the performance of the device for specific operating conditions. For more details, see the CHECKING LOOP STABILITY section.

In high-frequency converter applications, the efficiency is essentially affected by the inductor AC resistance (i.e. quality factor) and to a smaller extent by the inductor DCR value. To achieve high efficiency operation, care should be taken in selecting inductors featuring a quality factor above 25 at the switching frequency. Increasing the inductor value produces lower RMS currents, but degrades transient response. For a given physical inductor size, increased inductance usually results in an inductor with lower saturation current.

The total losses of the coil consist of both the losses in the DC resistance,  $R_{(DC)}$ , and the following frequency-dependent components:

- The losses in the core material (magnetic hysteresis loss, especially at high switching frequencies)
- Additional losses in the conductor from the skin effect (current displacement at high frequencies)
- Magnetic field losses of the neighboring windings (proximity effect)
- Radiation losses

For good efficiency, the inductor's DC resistance should be less than  $30m\Omega$ . The following inductor series from different suppliers have been used with the TPS6128x converters.

Table 7. List of Inductors

MANUFACTURER	SERIES	DIMENSIONS (in mm)	DC INPUT CURRENT LIMIT SETTING
	DFE252010C	2.5 x 2.0 x 1.0 max. height	≤3000 mA
	DFE252012C	2.5 x 2.0 x 1.2 max. height	≤3500 mA
	DFR252010C	2.5 x 2.0 x 1.0 max. height	≤3000 mA
TOKO	DFE252012C	2.5 x 2.0 x 1.2 max. height	≤3500 mA
TORU	DFE252012P	2.5 x 2.0 x 1.2 max. height	≤3500 mA
	DFE201610C	2.0 x 1.6 x 1.0 max. height	≤2000 mA
	DFE201612C	2.0 x 1.6 x 1.2 max. height	≤3000 mA
	DFE201612P	2.0 x 1.6 x 1.2 max. height	≤3000 mA

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#### **OUTPUT CAPACITOR**

For the output capacitor, it is recommended to use small ceramic capacitors placed as close as possible to the VOUT and GND pins of the IC. If, for any reason, the application requires the use of large capacitors which can not be placed close to the IC, using a smaller ceramic capacitor in parallel to the large one is highly recommended. This small capacitor should be placed as close as possible to the V<sub>OUT</sub> and GND pins of the IC. To get an estimate of the recommended minimum output capacitance, Equation 10 can be used.

$$C_{MIN} = \frac{I_{OUT} \cdot (V_{OUT} - V_{IN})}{f \cdot \Delta V \cdot V_{OUT}}$$
(10)

Where f is the switching frequency which is 2.3MHz (typ.) and  $\Delta V$  is the maximum allowed output ripple.

With a chosen ripple voltage of 20mV, a minimum effective capacitance of 10µF is needed. The total ripple is larger due to the ESR and ESL of the output capacitor. This additional component of the ripple can be calculated using Equation 11

$$\Delta V_{\text{OUT(ESR)}} = \text{ESR} \cdot \left( \frac{I_{\text{OUT}}}{1 - D} + \frac{\Delta I_{\text{L}}}{2} \right)$$
(11)

$$\Delta V_{\text{OUT(ESL)}} = \text{ESL} \cdot \left( \frac{I_{\text{OUT}}}{1 - D} + \frac{\Delta I_{\text{L}}}{2} - I_{\text{OUT}} \right) \cdot \frac{1}{t_{\text{SW(RISE)}}}$$
(12)

$$\Delta V_{\text{OUT(ESL)}} = \text{ESL} \cdot \left( \frac{I_{\text{OUT}}}{1 - D} - \frac{\Delta I_{\text{L}}}{2} - I_{\text{OUT}} \right) \cdot \frac{1}{t_{\text{SW(FALL)}}}$$
(13)

with:

- I<sub>OUT</sub> = output current of the application
- D = duty cycle
- ΔI<sub>1</sub> = inductor ripple current
- t<sub>SW(RISE)</sub> = switch node rise time
- t<sub>SW(FALL)</sub> = switch node fall time
- ESR = equivalent series resistance of the used output capacitor
- ESL = equivalent series inductance of the used output capacitor

An MLCC capacitor with twice the value of the calculated minimum should be used due to DC bias effects. This is required to maintain control loop stability. The output capacitor requires either an X7R or X5R dielectric. Y5V and Z5U dielectric capacitors, aside from their wide variation in capacitance over temperature, become resistive at high frequencies. There are no additional requirements regarding minimum ESR. Larger capacitors cause lower output voltage ripple as well as lower output voltage drop during load transients.

In applications featuring high (pulsed) load currents (e.g. ≥2Amps), it is recommended to run the converter with a reasonable amount of effective output capacitance and low-ESL device, for instance x2 22µF X5R 6.3V (0603) MLCC capacitors connected in parallel with a 1µF X5R 6.3V (0306-2T) MLCC LL capacitor.

DC bias effect: high cap. ceramic capacitors exhibit DC bias effects, which have a strong influence on the device's effective capacitance. Therefore the right capacitor value has to be chosen very carefully. Package size and voltage rating in combination with material are responsible for differences between the rated capacitor value and it's effective capacitance. For instance, a  $10\mu F$  X5R 6.3V (0603) MLCC capacitor would typically show an effective capacitance of less than  $5\mu F$  (under 3.5V bias condition, high temperature).

For RF Power Amplifier applications, the output capacitor loading is combined between the dc/dc converter and the RF Power Amplifier (x2 10µF X5R 6.3V (0603) + PA input cap 4.7µF X5R 6.3V (0402)) are recommended.

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High values of output capacitance are mainly achieved by putting capacitors in parallel. This reduces the overall series resistance (ESR) to very low values. This results in almost no voltage ripple at the output and therefore the regulation circuit has no voltage drop to react on. Nevertheless to guarantee accurate output voltage regulation even with very low ESR the regulation loop can switch to a pure comparator regulation scheme.

During this operation (COUTRNG bit = 1) the output voltage is regulated between two thresholds. The upper threshold is defined by the programmed output voltage and the lower value is about 10mV lower. If the upper threshold is reached the off-time is increased to reduce the current in the inductor. Therefore the output voltage will slightly drop until the lower threshold is tripped. Now the off-time will be reduced to increase the current in the inductor to charge up the output voltage to the steady-state value. The current swing during this operation mode is strongly depending on the current drawn by the load but will not exceed the programmed current limit. The output voltage during comparator operation stays within the specified accuracy with minimum voltage ripple.

#### INPUT CAPACITOR

Multilayer ceramic capacitors are an excellent choice for input decoupling of the step-up converter as they have extremely low ESR and are available in small footprints. Input capacitors should be located as close as possible to the device. While a 4.7µF input capacitor is sufficient for most applications, larger values may be used to reduce input current ripple without limitations.

Take care when using only ceramic input capacitors. When a ceramic capacitor is used at the input and the power is being supplied through long wires, such as from a wall adapter, a load step at the output can induce ringing at the VIN pin. This ringing can couple to the output and be mistaken as loop instability or could even damage the part. Additional "bulk" capacitance (electrolytic or tantalum) should in this circumstance be placed between  $C_l$  and the power source lead to reduce ringing than can occur between the inductance of the power source leads and  $C_l$ .

#### **CHECKING LOOP STABILITY**

The first step of circuit and stability evaluation is to look from a steady-state perspective at the following signals:

- Switching node, SW
- Inductor current, I<sub>1</sub>
- Output ripple voltage, V<sub>OUT(AC)</sub>

These are the basic signals that need to be measured when evaluating a switching converter. When the switching waveform shows large duty cycle jitter or the output voltage or inductor current shows oscillations, the regulation loop may be unstable. This is often a result of board layout and/or L-C combination.

As a next step in the evaluation of the regulation loop, the load transient response is tested. The time between the application of the load transient and the turn on of the P-channel MOSFET, the output capacitor must supply all of the current required by the load.  $V_{OUT}$  immediately shifts by an amount equal to  $\Delta I_{(LOAD)}$  x ESR, where ESR is the effective series resistance of  $C_{OUT}$ .  $\Delta I_{(LOAD)}$  begins to charge or discharge  $C_{OUT}$  generating a feedback error signal used by the regulator to return  $V_{OUT}$  to its steady-state value. The results are most easily interpreted when the device operates in PWM mode.

During this recovery time,  $V_{OUT}$  can be monitored for settling time, overshoot or ringing that helps judge the converter's stability. Without any ringing, the loop has usually more than 45° of phase margin. Because the damping factor of the circuitry is directly related to several resistive parameters (e.g., MOSFET  $r_{DS(on)}$ ) that are temperature dependant, the loop stability analysis has to be done over the input voltage range, load current range, and temperature range.

4 Submit Documentation Feedback



#### LAYOUT CONSIDERATIONS

For all switching power supplies, the layout is an important step in the design, especially at high peak currents and high switching frequencies. If the layout is not carefully done, the regulator could show stability problems as well as EMI problems. Therefore, use wide and short traces for the main current path and for the power ground tracks.

To minimize voltage spikes at the converter's output, it is advisable to place the output capacitor(s) as close as possible to GND and  $V_{OUT}$ , as shown in Figure 53. The input capacitor and inductor should also be placed as close as possible to the IC. Use a common ground node for power ground and a different one for control ground to minimize the effects of ground noise. Connect these ground nodes at any place close to the ground pins of the IC.

Junction-to-ambient thermal resistance is highly application and board-layout dependent. It is suggested to maximize the pour area for all planes other than SW. Especially the ground pour should be set to fill available PWB surface area and tied to internal layers with a cluster of thermal vias.

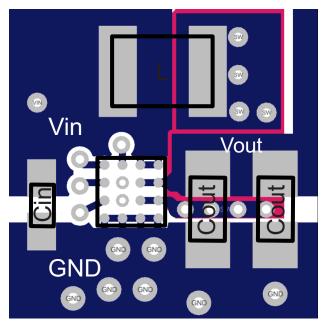


Figure 53. Suggested Layout (Top)



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#### THERMAL INFORMATION

Implementation of integrated circuits in low-profile and fine-pitch surface-mount packages typically requires special attention to power dissipation. Many system-dependent issues such as thermal coupling, airflow, added heat sinks and convection surfaces, and the presence of other heat-generating components affect the powerdissipation limits of a given component.

Three basic approaches for enhancing thermal performance are listed below:

- Improving the power dissipation capability of the PCB design
- Improving the thermal coupling of the component to the PCB
- Introducing airflow in the system

As power demand in portable designs is more and more important, designers must figure the best trade-off between efficiency, power dissipation and solution size. Due to integration and miniaturization, junction temperature can increase significantly which could lead to bad application behaviors (i.e. premature thermal shutdown or worst case reduce device reliability).

Junction-to-ambient thermal resistance is highly application and board-layout dependent. In applications where high maximum power dissipation exists, special care must be paid to thermal dissipation issues in board design. The device operating junction temperature (T<sub>J</sub>) should be kept below 125°C.

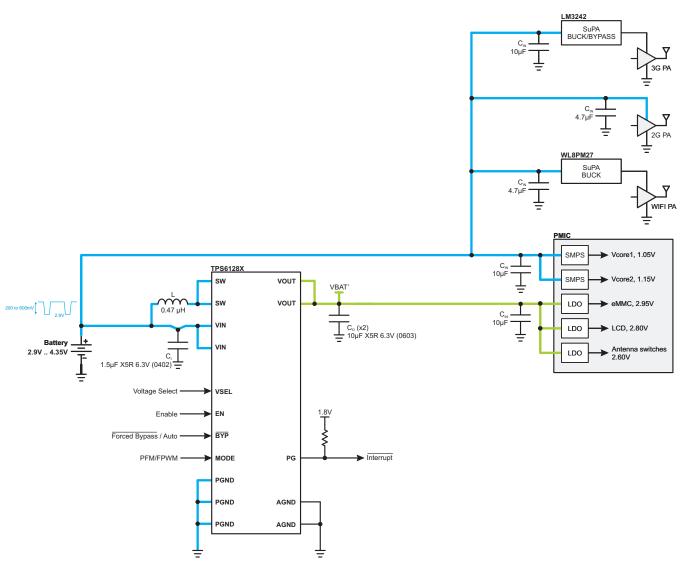


Figure 54. TPS6128x PMIC Pre-Regulator (ILIM = 2000mA)
Li-lon Battery Application with Extended Voltage Range, 2G Radio Tx Back-Off (at Low Battery Voltage)

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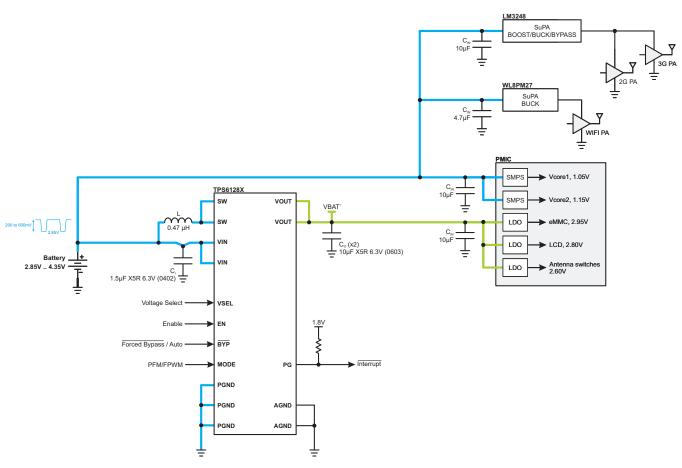


Figure 55. TPS6128x PMIC Pre-Regulator (ILIM = 2000mA)
Si-Anode Battery Application with Extended Voltage Range, Full Featured 2G/3G Radio Performance

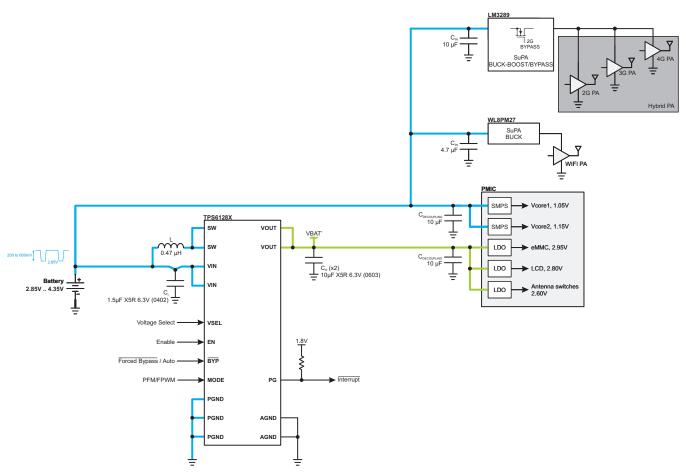


Figure 56. TPS6128x PMIC Pre-Regulator (ILIM = 2000mA) Li-lon Battery Application with Extended Voltage Range Full Featured 3G/4G Radio Performance (Best Efficiency) 2G Radio Tx Back-Off (at Low Battery Voltage)



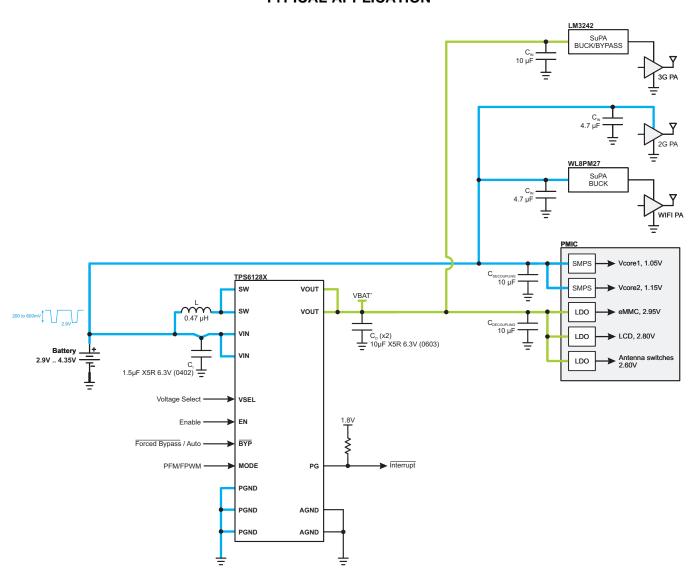


Figure 57. TPS6128x PMIC Pre-Regulator (ILIM = 2500mA) Low Cost, Li-Ion Battery Application with Extended Voltage Range 3G Radio Support, 2G Radio Tx Back-Off (at Low Battery Voltage)

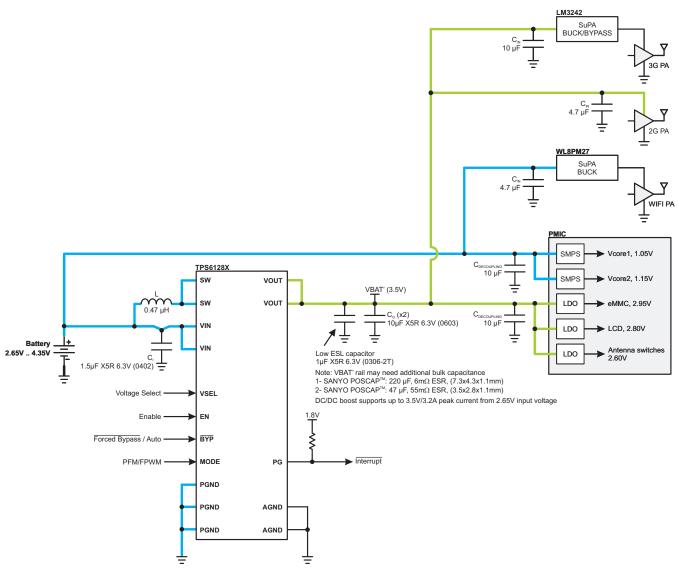
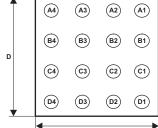


Figure 58. TPS6128x PMIC Pre-Regulator (ILIM = 5000mA)
Low Cost, Si-Anode Battery Application with Extended Voltage Range, 2G/3G Radio Support



#### **PACKAGE SUMMARY**

# CHIP SCALE PACKAGE (BOTTOM VIEW)



# CHIP SCALE PACKAGE (TOP VIEW)



#### Code:

- YM Year Month date code
- LLLL Lot trace code
- S Assembly site code

#### **CHIP SCALE PACKAGE DIMENSIONS**

The TPS6128x device is available in a 16-bump chip scale package (YFF, NanoFree™). The package dimensions are given as:

- D = ca. 1666 ±30 µm
- E = ca. 1666 ±30 μm





29-Oct-2013

#### PACKAGING INFORMATION

Orderable Device	Status	Package Type	Package Drawing		Package Qty	Eco Plan	Lead/Ball Finish	MSL Peak Temp	Op Temp (°C)	Device Marking (4/5)	Samples
TPS61280YFFR	ACTIVE	DSBGA	YFF	16	3000	Green (RoHS & no Sb/Br)	SNAGCU	Level-1-260C-UNLIM	-40 to 85	TPS 61280	Samples
TPS61280YFFT	ACTIVE	DSBGA	YFF	16	250	Green (RoHS & no Sb/Br)	SNAGCU	Level-1-260C-UNLIM	-40 to 85	TPS 61280	Samples
TPS61281YFFR	ACTIVE	DSBGA	YFF	16	3000	Green (RoHS & no Sb/Br)	SNAGCU	Level-1-260C-UNLIM	-40 to 85	TPS 61281	Samples
TPS61281YFFT	ACTIVE	DSBGA	YFF	16	250	Green (RoHS & no Sb/Br)	SNAGCU	Level-1-260C-UNLIM	-40 to 85	TPS 61281	Samples
TPS61282YFFR	ACTIVE	DSBGA	YFF	16	3000	Green (RoHS & no Sb/Br)	SNAGCU	Level-1-260C-UNLIM	-40 to 85	TPS 61282	Samples
TPS61282YFFT	ACTIVE	DSBGA	YFF	16	250	Green (RoHS & no Sb/Br)	SNAGCU	Level-1-260C-UNLIM	-40 to 85	TPS 61282	Samples

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check http://www.ti.com/productcontent for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

**Pb-Free** (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes. **Pb-Free** (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between

the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.



# **PACKAGE OPTION ADDENDUM**

29-Oct-2013

(6) Lead/Ball Finish - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

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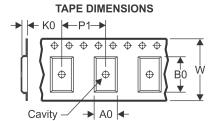
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# PACKAGE MATERIALS INFORMATION

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# TAPE AND REEL INFORMATION





_		
		Dimension designed to accommodate the component width
		Dimension designed to accommodate the component length
		Dimension designed to accommodate the component thickness
	W	Overall width of the carrier tape
ſ	P1	Pitch between successive cavity centers

#### QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



#### \*All dimensions are nominal

All dimensions are nominal												
Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPS61280YFFR	DSBGA	YFF	16	3000	180.0	8.4	1.78	1.78	0.69	4.0	8.0	Q1
TPS61280YFFT	DSBGA	YFF	16	250	180.0	8.4	1.78	1.78	0.69	4.0	8.0	Q1
TPS61281YFFR	DSBGA	YFF	16	3000	180.0	8.4	1.78	1.78	0.69	4.0	8.0	Q1
TPS61281YFFT	DSBGA	YFF	16	250	180.0	8.4	1.78	1.78	0.69	4.0	8.0	Q1
TPS61282YFFR	DSBGA	YFF	16	3000	180.0	8.4	1.78	1.78	0.69	4.0	8.0	Q1

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\*All dimensions are nominal

7 il difficiolo de fiornifici											
Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)				
TPS61280YFFR	DSBGA	YFF	16	3000	182.0	182.0	17.0				
TPS61280YFFT	DSBGA	YFF	16	250	182.0	182.0	17.0				
TPS61281YFFR	DSBGA	YFF	16	3000	182.0	182.0	17.0				
TPS61281YFFT	DSBGA	YFF	16	250	182.0	182.0	17.0				
TPS61282YFFR	DSBGA	YFF	16	3000	182.0	182.0	17.0				

E: Max = 1.696 mm, Min =1.636 mm

<del>4207625 8/AN 07/1</del>5

# DIE-SIZE BALL GRID ARRAY YFF (S-XBGA-N16) 0,40 0,40 0,20 В $\oplus$ В Α 0,20 2 PIN A1 INDEX AREA SEATING PLANE △|0,05|C| D: Max = 1.696 mm, Min = 1.636 mm

NOTES: A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994.

- B. This drawing is subject to change without notice.
- C. NanoFree™ package configuration.

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